Mechanical behavior of tubular welded T-joints with circular and elliptical cross-sections

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Abstract: The aim of this work is to analyze, numerically, the elastic and elastoplastic behavior of three tubular T-joints with different cross-sections of braces. The first one is circular and the others are elliptical but assembled differently (longitudinal and transversal positions). The elastic study is to compare, in three charge cases, the geometric stress variation around the weld toe for the three T-joints. In the elastoplastic study, the limit loads of these joints were compared for each load case. In the order to facilitate interpretations, the results are presented in graphical form. The numerical simulations are performed using Patran and Nastran softweres. **Keywords :** Circular cross-section, Elasticity, Elastoplasticity, Elliptical cross-section, Hot spot, Limit load.

I. INTRODUCTION

The tubular welded joints find applications in many fields of mechanical engineering. We quote: water pipes, tripods, gateways and offshore platform supports. These supports are mainly formed by a set of structural element welded together to form tubular joints with different geometrical configurations (T, Y, K, KT, DT, DY, DK, DKT, ...). In the most cases, the structural elements are tubes with circular cross-sections. Hence the idea to compare elastic and elastoplastic responses of these kinds of joints with others which the braces have elliptical cross-sections.

Several studies have been addressed to analyze the tubular welded joint behaviors. In [1], Ghanameh et al. have carried out the simulations to evaluate the local stress variation in the vicinity of toe weld linking chords and braces. This is carried for several kinds of planar joints with circular cross-sections under combined loading. In [2], Lee studied firstly, the T and Y-joints under tensile loading, in plane and out plane bending. Secondly, the K and DT-joint under balanced loading. Soh et al. [3] have also studied the DT, K and KT-joints in three cases of balanced loads, TEN, IPB and OPB. In [4], a comparative study of elastic and elastoplastic behaviors for T, Y, DT and DY-joints was performed. This study found that the joints with inclined braces are more robust than those having perpendicular braces. This is valid for elastic and elastoplastic studies. In [5], an analysis of the influence of the geometrical parameters of the stress concentration factor was performed. This study was undertaken for tubular KT-joints with circular cross-sections but with internal stiffeners. In this work, it was noted that the authors have introduced a new adimensional parameter which is directly proportional to the size of the stiffeners. The study of numerical simulation, which the mesh has been validated experimentally, has shown that the SCF decreases when the new parameter increases.

II. CHOICE OF JOINTS AND BOUNDARY CONDITIONS

Three specimens named T_1 , T_2 and T_3 will be studied in this work. They have identical chords with circular cross-sections. The brace of T_1 has a circular cross-section, T_2 and T_3 have braces with elliptical cross-sections of the same dimensions but they are arranged differently (Fig. 8).

For each specimen, three load cases will be treated, tensile loading (TEN), in plane bending (IPB) and out plane bending (OPB). The loads will be applied at the free ends of braces. The ends of the chords are, all the time, fixed.



Fig. 1 – Mesh of quadrilateral thin shell elements with four nodes: (a) T₁-joint, (b) T₂-joint, (c) T₃-joint

The mesh is made using Patran software, while post-processing is handled using Nastran software. For the three specimens, the vicinity of the weld is subdivided into 96 finite elements in the aim to collect the maximum stresses values along the weld toe (Fig. 1).

The material chosen for this study is the construction steel of Young's modulus 2.1×10^{5} MPa, yeld point 240MPa and Poisson's ratio 0.33. For the elastoplastic study which we determine the limit loads, the material will be considered elastic perfectly plastic.

III. ELASTIC BEHAVIOR OF JOINTS

The three specimens T_1 , T_2 and T_3 are submitted independently to three kinds of external loads, TEN, IPB and OPB. For each load case, will be presented in same graph the local stress evolution σ_L in term of the angle ψ . This is for the three joints.

Tensile loading

In the case of tensile loading, a force equal to 10^4 N is applied to the brace's free end. For the three kinds of joints studied, we note that the hot spot is located at the Saddle with 194MPa, 185MPa and 208MPa for T1, T2 and T3 respectively. We note that in the vicinity of the saddle, the T₃-joint has the highest local stress value (Fig. 2). But apart from this location, the local stress of T₂ is predominates. We also note that the smallest value of the local stress is recorded in the Crown; this is for the three specimens.



Fig. 2 – Evolution of the local stress around the weld toe following a tensile force of 10kN applied at the brace's free end

Loading of in plan bending

In this load case, in plane bending is applied at the free end of the brace. As in the case of tensile, the curve of the T_1 -joint is always between these of T_2 and T_3 -joints. But in the vicinity of Crown, the curves for T_1 and T_3 -joints are almost confounded, i.e. we also note that the Crown and its neighborhood are a hot area for all specimens with a predominance of T_2 which admits a maximum stress equal to 216MPa (Fig. 3). Conversely,

compared to tensile case, the stress of T_2 -joint is dominant in the hot area. Far from this location, the geometrical stress of the T_3 -joint is the biggest.



Fig. 3 – Evolution of the local stress around the weld toe following IPB of 2.5kN applied at the brace's free ends

Loading of out plan bending

The three joints are solicited with an external force equal to 1kN applied to the brace's free end perpendicularly to the symmetry plane of the specimens. We note that the hot spots are located at the saddle, for three specimens, like the tensile case. We also note that the local stress of the T_1 -joint is between those for T_2 and T_3 -joints with a predominance of T_2 throughout the weld. T_1 and T_3 -joints have almost the same value of the local stress at the hot spot (Saddle in this case) which is equal to 212MPa. At the Crown, all specimens have approximately the same value of the geometrical stress (local) which is about 13MPa (Fig. 4).



Fig. 4 – Evolution of the local stress around the weld toe following OPB of 1kN applied at the brace's free ends

IV. ELASTOPLASTIC BEHAVIOR OF JOINTS

The aim of this work is to levy the force applied to the brace's free end in term of displacement. This will be performed in three load cases, TEN, IPB and OPB for each specimen. To facilitate comparison, the results will be exposed graphically. The first observation we can make is that all curves tend to a limit load whatever the load and for all joints.

Tensile loading

In this case load, we note that the curve for T_1 -joint is located between the other two curves with a predominance of T_3 -joint. We also note that the limit load of the T_1 -joint is equal to 87kN while those T_2 -joint and T_3 -joint are equal to 74kN and 93kN respectively (Fig. 5).



Fig. 5 – Variation of the tensile force in term of the displacement of the brace's free end

Loading of in plane bending

In this load case, we note that T_1 and T_2 -joints have the same elastoplastic responses, i.e. they have the same load limit which is equal to 11kN. This value is higher than recorded for T_3 -joint which is equal to 9.8kN (Fig. 6).



Fig. 6 - Variation of the IPB loading in term of the displacement of the brace's free end

Loading out plane bending

The elastoplastic response in this case load is similar to the tensile case, i.e. the curve of T_1 -joint is between T_2 and T_3 -joint with predominance of T_3 . The limit loads of T_1 , T_2 and T_3 -joints are equal to 5kN, 6.8kN and 8.8kN respectively (Fig. 7).



Fig. 7 - Variation of the OPB loading in term of the displacement of the brace's free end

V. CONCLUSIONS

The elastic study of three joints T_1 , T_2 and T_3 led to the following conclusions:

- In the TEN and OPB load cases, whatever the shape of the brace cross-section, the hot spot is located at the Saddle.

- In the IPB load case, the hot areas coincide with Crown and its vicinity whatever the shape of the brace cross-section.

- The joints with circular braces and with longitudinal elliptical braces have the same SCF under IPB loading.

- Around the toe weld, the geometric stress of the joints with circular brace is, all the time, between those with the elliptical braces. This is for all loading cases.

The elastoplastic study for T_1 , T_2 and T_3 -joints led to the following conclusions:

- In the TEN and OPB load cases, the limit load of the joint with circular brace is, all the time, between those with the elliptical braces.

- The joints with circular and longitudinal elliptical braces have the same limit load under IPB loading.

- For all joints and all load cases, the limit load in the IPB load case is more important to compare with IPB load case.

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Fig. 8 – T-joints : (a) T-joint with circular brace T_1 , (b) T-joint with longitudinal elliptical brace T_2 , (c) T-joint with Transversal elliptical brace T_3 .

- TEN : Tensile load
- IPB : In Plane Bending
- OPB : Out Plane Bending
- D : Outside diameter of chord
- d : Outside diameter of brace
- T : Chord's thickness
- t : Brace's thickness
- L : Chord's length
- 1 : Brace's length
- ψ : Angle orienting the weld measured from Crown
- σ_L : Local Stress
- SFC : Stress Factor Concentration