

# Analysis And Design Of Multi Storey Building By Using “STAADPRO”

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## **Abstract:**

A review of the analysis and design of a multi-storey building with STAAD Pro is carried out. Planning is done by using AutoCAD and load calculations were done manually and then the structure was analysed using STAAD Pro . The dead load , imposed load and wind load with load combination are calculated and applied to the structure. Overall , the concepts and Procedures of designing the essential components of a multi-storey building are described . STAAD Pro software also gives a detailed value of shear force , bending moment and torsion of each element of the structure which is with in IS code limits.

**Keywords:** STAAD Pro, Multi-storey building, dead load, imposed load, wind load, Shear force, bending moment, torsion, IS code limits.

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## I. Introduction

Now a days tall or multi-storey buildings has gain very much importance, because in metro Cities there is a rapid increase in population with limited land.

All people require good accommodations, aesthetic, comfort and safety. That's the reason for increase in construction of multi-storey buildings.

Structural design of multi-storey buildings is basically worried with safety during ground motion, serviceability what's more, potential for monetary mis fortune.

Design of structures using Limit State method Design the members are designed for the limiting bending moment and Service ability limits, hence the structures are left with minimum reserve energy. Earthquake Will cause more severe effect on tall buildings compare to small buildings. Due to earthquake .A symmetrical buildings will damage more than symmetrical buildings. In case of high rise structures horizontal loads produce develop high lateral displacements which is not desirable for the occupants and the structure itself. The enormous increase in population and scarcity of land makes the people to move from rural Areas to urban paces and construction of multi-storied buildings in small areas is being common now-a-days.

Functional designing of the building has become very important and the requirements vary from one building to another .

Every Civil Engineer should know the usage of the Buildings by contacting the people and basic principles of designing of the R.C.C structures.

This project is intended at Analyzing and designing the multi-storey structure using STAAD.PRO.V8i and STAAD.ETC. In this project, we adopted limitstate method of analysis and Design the structural members manually and using STAAD.PRO.V8i and STAAD.ETC .Manually design is done for particular beam, column and slab by using IS456:2000 and load sare dead load, imposed load and external load considered according to IS875:1987 (PARTIII).

It is the checked in STAAD.PRO.V8i and STAAD.

## II. Objectives

The study aims to Analysis and design of the RCC frame structure apply Load Combination as Live load, dead load, wind load and other earthquake . These objectives are defined as follows:

Analysis of the Structure of G+5 Building Live load and Dead Load.

Analysis of the Structure of G+5 Building Wind load ,Earthquake Load and Seismic Load .

C) Generating structural framing plan .

D) Creating 3D Structural Model in STAAD PRO .

E) Analysis of the Structure with Apply All Load combination.

F) Design of G+5 RCC frame structure .

### III. Literature Review

- A) Ibrahim,et.al(April2019)1: Design and Analysis of Residential Building(G+ 4):
- B) Dunnala Lakshmi Anuja,et.al (2019) 2: Planning, Analysis and Design of Res-Identical Building(G+ 5)By using STAAD Pro:
- C) Mr K.Prabin Kumar,et.al(2018)3:
- D) Deevi Krishna Chaitanya,et.al(January,2017)4:Analys is and Design of a (G+ 6)Multi-Storey Building Using STAAD Pro:
- E) R. D. Deshpande, et. Al (June,2017)5: Analysis, Design and Estimation of Basement+ G+ 2 Residential Building:

### IV. Methodology

#### About Staad Pro

Our project involves analysis and design of multi-storeyed[G+ 5]using a very popular designing Software STAADPro.We have chosen STAAD Pro because of its following.

#### Advantages

- easy to use interface,
- conformation with the Indian Standard Codes,
- versatile nature of solving any type of problem,
- Accuracy of the solution.

STAAD.Pro features a state-of-the-art user interface,visualization tools,and powerful analy-sis and design engines with advanced finite element and dynamic analysis capabilities.From model generation,analysis and design to visualization and result verification,STAAD.Pro is the professionals choice for steel,concrete,timber,aluminium and cold-formed steel design of low and high-rise buildings,culverts,petrochemical plants,tunnels,bridges,piles and much more.

To start with we have solved some sample problem susing STAAD Pro and checked the accuracy of the results with manual calculations.The results were to satisfaction and were accurate.In the initial phase of our project we have done calculations regarding loadings on buildings and also considered seismic and wind loads.

Structural analysis comprises the set of physical laws and mathematics required to study and predicts the behaviour of structures.Structur alanalysis is can be viewed more abstractly as a method to drive the engineering design process or prove the soundness of a design with out a dependence on directly testing it.

To perform an accurate analysis a structural engineer must determine such in formation as structural loads,geometry,support conditions,and materials properties.The results of such ananalysis typically include support reactions,stresses and displacements.This informationis then compared to criteria that indicate the conditions of failure.Advanced structural analysismay examine dynamic response,stability and non-linear behavior.

#### Loads Considered

**1.Dead load:-** The unit weights of plain concrete and reinforced Concrete made with sand and gravel or crushed natural stone aggregate may be taken as 24 kN/ m<sup>2</sup>and 25 kN/ m<sup>2</sup>respectively.

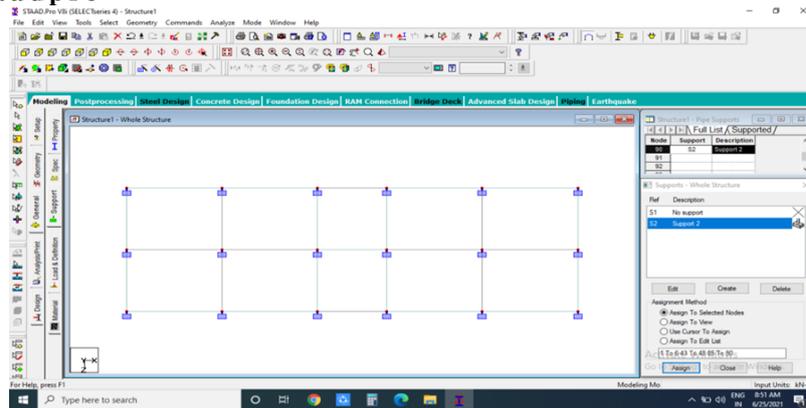
**2.Imposed load:-** Imposed load is produced by the intended use or occupancy of a building in cluding the weight of movable partitions ,distributed and concentrated Loads due to the impact and vibration and dust loads.

**3.Wind load:-** The wind speeds are assessed with the aidofanemometers or Anemographs which are installed at meteorological observatories at heights generally varying from 10 to 30 meters above ground.

**4.Secmic load:-** According to the severity of earthquake intensity they are divided in to zones.

- 1.ZoneIandIIarecombinedaszoneII.
- 2.ZoneIII.
- 3.ZoneIV.
- 4.ZoneV.

## Working With Staad pro



### Plan of G+5 storey building

All columns= 0.40\*0.60m

All beams= 0.3\*0.5m

All slabs= 0.125mthick

### Physical parameters of building

Length= 4 bays @5.5m+ 1 bay@4m= 26m

Width= 2 bays @4m= 8.0m

Height= 3m+ 5 storeys @3.5m= 20.5m

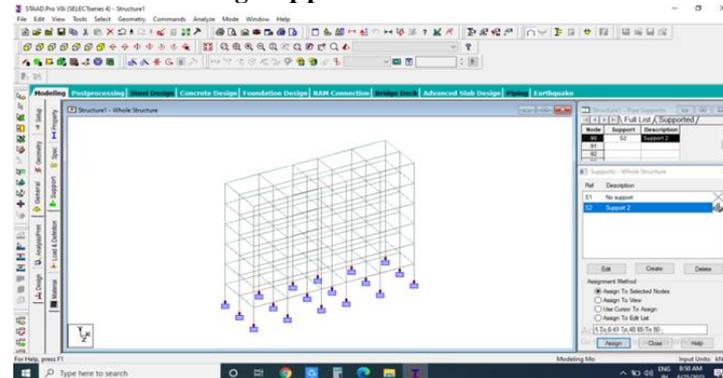
Live load on the floors is 2kN/ m<sup>2</sup>

Live load on the roof is 1.5kN/ m<sup>2</sup>

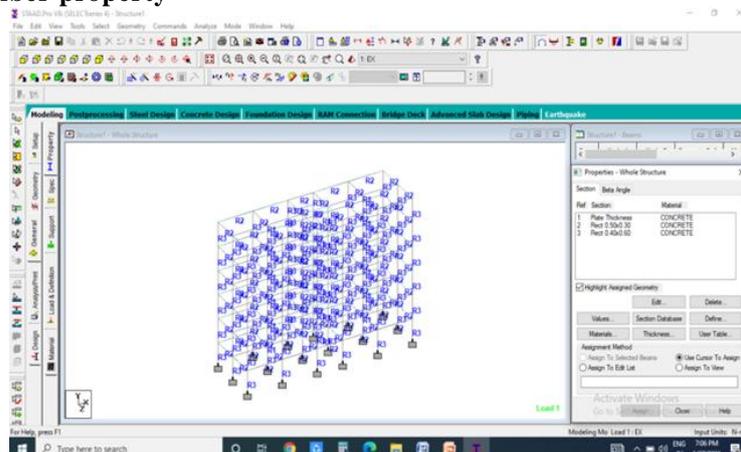
Grade of concrete and steel used

Used M 25 concrete and Fe 415 steel

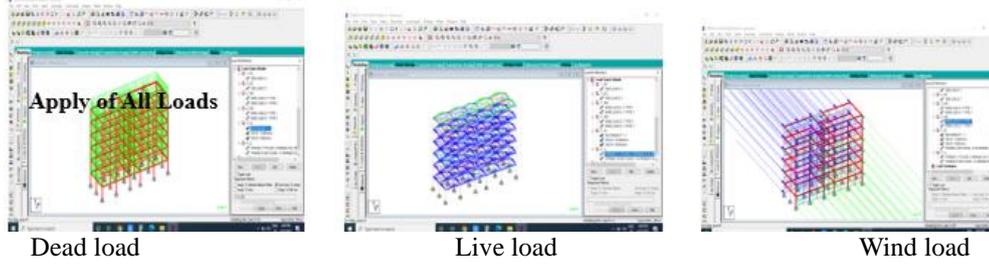
### Generation of the structure & Fixing support of structure



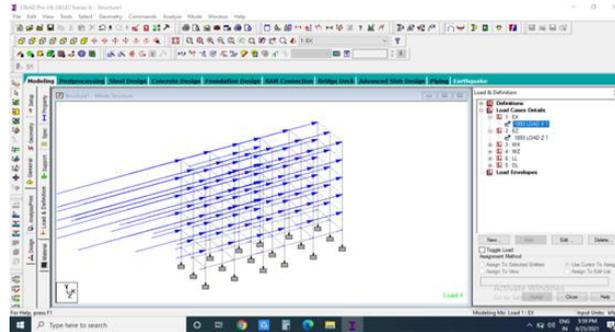
### Generation of member property



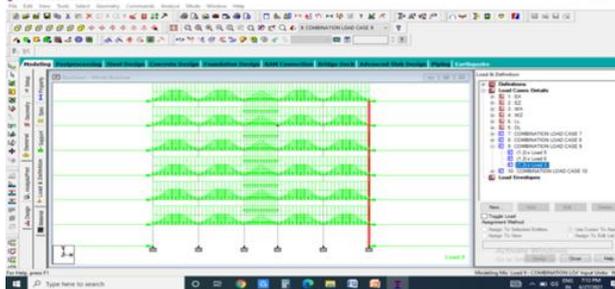
Apply of All Loads



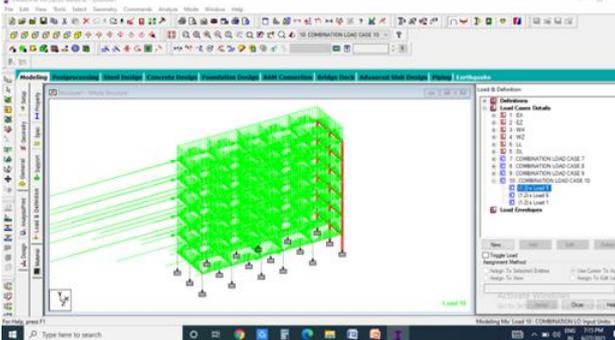
Structure under seismic load



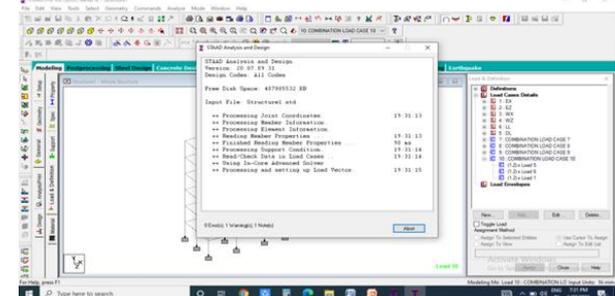
Combination under wind load



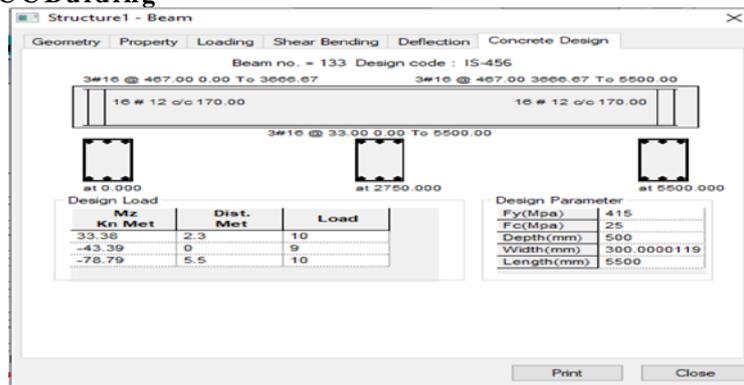
Combination under Seismic load



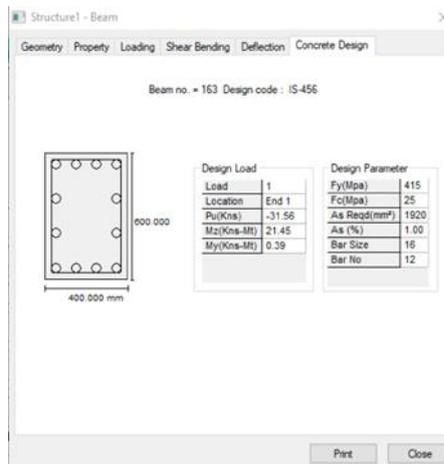
Showing the analyzing window



**Design of G + 5 RCC Bulding**

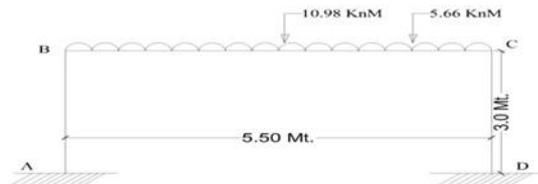


**Beam Design**



**Column Design**

Manual Analysis (Kanis Method)



Step1: Fixed End Moments

MFAB, MFBA, MFCD, MFDC= 0

MFBC=  $-wl^2/ 12 = -10.985.52/ 12 - 5.665.52/ 12 = -41.946\text{KNm}$

Step2: Rotation Factor

Joint	Member	Relativestiffness(k)	summK	RF= $-0.5(k/ \text{summK})$
B	BA	$(4EI/ l) = 1.33EI$	2.057EI	-0.323
-	BC	$(4EI/ l) = 0.727EI$	-	-0.176
C	CB	$(4EI/ l) = 0.727EI$	2.057EI	-0.176
-	CD	$(4EI/ l) = 1.33EI$	-	-0.323

Step3: Kanis scheme and Rotation Contribution

Rotation Contribution=  $RF[FEM + \text{Near end contribution} + \text{Far end contribution}]$

RCforBA1=  $-0.323[-41.946 + 0 + 0] = 13.54$

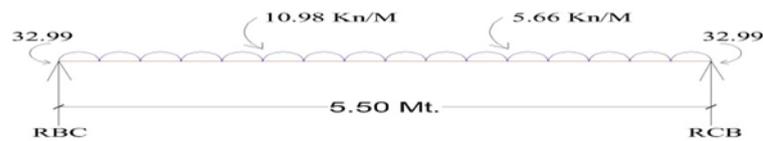
RCforBC1=  $-0.176[-41.946 + 0 + 0] = 7.38$

$RC_{forCB1} = -0.176[41.946 + 7.38 + 0] = -8.68$   
 $RC_{forCD1} = -0.323[41.946 + 7.38 + 0] = -15.93$   
 $RC_{forBA2} = -0.323[-41.9468.68 + 0] = 16.35$   
 $RC_{forBC2} = -0.176[-41.9468.68 + 0] = 8.91$   
 $RC_{forCB2} = -0.176[41.946 + 8.91 + 0] = -8.95$   
 $RC_{forCD2} = -0.323[41.946 + 8.91 + 0] = -16.42$   
 $RC_{forBA3} = -0.323[-41.9468.95 + 0] = 16.43$   
 $RC_{forBC3} = -0.176[-41.9468.95 + 0] = 8.95$   
 $RC_{forCB3} = -0.176[41.946 + 8.95 + 0] = -8.95$   
 $RC_{forCD3} = -0.323[41.946 + 8.95 + 0] = -16.43$

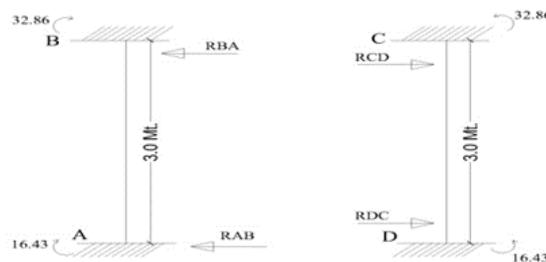
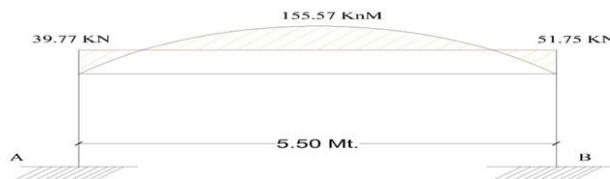
**Step4: FinalMoments**

Joint	A	B	B	C	C	D
Members	AB	BA	BC	CB	CD	DC
FEM	0	0	-41.946	-41.946	0	0
2NEM	0	32.86	17.9	-17.9	-32.86	0
2FEM	16.43	0	-8.95	8.95	0	-16.43
FinalMoments	16.43	32.86	-32.99	32.99	-32.86	-16.43

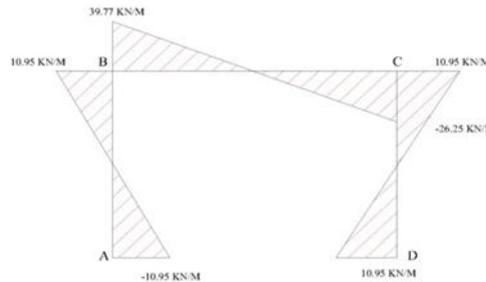
Summ Mbc= 0



$-R_{cb} * 5.5 + 32.99 + 5.66 * 5.5 * 2.75 + 10.98 * 5.5 * 2.75 = 0$   
 $R_{cb} = 51.75 \text{ KN/m}$   
 Summ V = 0  
 $R_{bc} + R_{cb} = 10.98 * 5.5 + 5.66 * 5.5$   
 $R_{bc} = 91.52 - 51.75 = 39.77 \text{ KN/m}$   
 BM at center,  $91.52 * 2.75 - 32.99 - 10.98 * 2.75 * 1.375 - 5.66 * 2.75 * 1.375 = 155.77 \text{ KNm}$



$-R_{ba} \cdot 3 + 32.86 = 0$   
 $R_{ba} = 10.95 \text{ KN/m}, R_{ab} = -10.95 \text{ KN/m}$   
 $R_{cd} \cdot 3 - 32.86 = 0$   
 $R_{cd} = 10.95 \text{ KN/m}, R_{dc} = -10.95 \text{ KN/m}$   
 For Bc, at 0m,  $R_{bc} = 39.77 \text{ KN/m}$   
 At 5.5m,  $R_{bc} = 10.95 \cdot 5.5 - 5.66 \cdot 5.5 = -26.28 \text{ KN/m}$



**Beam Design (IS456:2000)**

Width of support = 400mm  
 Clearspan = 5.5m  
 Load =  $21.16 \text{ KN/m}^2$   
 $b = 300 \text{ mm}, D = 500 \text{ mm}$   
 $f_{ck} = 25 \text{ N/mm}^2, f_y = 415 \text{ N/mm}^2$

**Step1: Effective Length**

$d = D_d = 500 - 25 = 475 \text{ mm}$   
 1. clear span + Effective depth =  $5.5 + 0.475 = 5.975 \text{ m}$   
 2. clear span + c/c distance between supports =  $5.5 + 0.2 + 0.2 = 5.9 \text{ m}$

**Step2: Ultimate Moment**

Self Weight of Beam ( $W_b$ ) =  $b \cdot D \cdot 25 = 0.3 \cdot 0.5 \cdot 25 = 3.75 \text{ KN/m}$   
 Total load ( $W$ ) =  $W_b + w = 3.75 + 21.16 = 24.98 \text{ KN/m}$   
 Now, Ultimate Load ( $w_u$ ) =  $1.5 \cdot 24.98 = 37.337 \text{ KN/m}$   
 Now, Ultimate Moment ( $M_u$ ) =  $W_u l^2 / 8 = 37.337 \cdot 5.9^2 / 8 = 162.63 \text{ KNm}$   
 Now, From page 96 IS456  
 $M_{u\text{lim}} = 0.138 \cdot f_{ck} b d^2 = 0.138 \cdot 25 \cdot 300 \cdot 475^2 = 233.52 \text{ KNm}$   
 $M_u$  less than  $M_{u\text{lim}}$ , Hence it is Under reinforced beam

**Step3: Calculation of area of steel**

$M_u = 0.87 f_y A_{st} d [1 - (f_y A_{st} / f_{ck} b d)] 162.63 \cdot 10^6 = 0.87 \cdot 415 \cdot A_{st} \cdot 475 \cdot [1 - (415 \cdot A_{st} / 25 \cdot 300 \cdot 475)]$   
 $A_{st} = 1085.56 \text{ mm}^2$   
 Using 20 mm dia bars,  $a_{st} = (\pi / 4) \cdot 20^2 = 314.45 \text{ mm}^2$   
 No of bars =  $(A_{st} / a_{st}) = (1085.56 / 314.45) = 3.45 = 3$   
 Provide 3no 20mm dia bars  
 Actual  $A_{st} = 3 \cdot (\pi / 4) \cdot 20^2 = 942.47 \text{ mm}^2$   
 Min  $A_{st} = 0.85 b d / f_y = (0.85 \cdot 300 \cdot 475) / 415 = 291.86 \text{ mm}^2$   
 Max  $A_{st} = 0.04 b d = 0.04 \cdot 300 \cdot 475 = 6000 \text{ mm}^2$

**Step4: Shear Reinforcement**

Factored Shear force =  $W_u l / 2 = 37.377 \cdot 5.9 / 2 = 110.26 \text{ KN/m}$   
 From page 72, IS 456,  
 Nominal shear stress ( $T_v$ ) =  $(V_u / b d) = (110.26 \cdot 10^3 / 300 \cdot 475) = 0.77 \text{ N/mm}$   
 Now, % of tension Reinforcement  
 $P = (A_{st} / b d) \cdot 100 = (942.47 / 300 \cdot 475) \cdot 100 = 0.66\%$

**Step5: Design Shear strength of concrete**

Page 73, table 19 IS 456 0.50, 0.49, 0.75, 0.57

By interpolation,  $T_c = 0.49 + ((0.57 - 0.49) / (0.75 - 0.50)) * (0.66 - 0.5)$

$T_c = 0.54 \text{ N/mm}$ ,  $T_v$  greater than  $T_c$ , Shear reinforcement required

**Step 6 Shear Reinforcement**

$V_{uc} = T_{cbd} = 0.54 * 300 * 475 = 76.95 \text{ KN}$

Now, Shear to be carried by stirrups

$V_{us} = V_u - V_{uc} = 110.267695 - 76.95 = 33.31 \text{ KN}$

Provide 8mm diameter 2legged vertical stirrups

$A_{sv} = (\pi/4) * 8^2 * 2 = 100.53 \text{ mm}^2$

Spacing  $S_v = (0.87 * 415 * 100.53 * 475 / 33.31 * 1000) = 517.5 \text{ mm}$

From page 48, IS 456,

1. Minimum Spacing =  $(A_{sv} / b S_v) * (0.4 / 0.87 f_y)$   $S_v = (A_{sv} * 0.87 f_y / 0.4 b) = (100.53 * 0.87 * 415 / 0.4 * 300)$

2. Spacing =  $0.75 d = 0.75 * 475 = 356.25 \text{ mm}$

3. 300mm Provide 8 mm dia 2 legged vertical stirrups @ 300mm c/c spacing.

**Step7: Check for Deflection**

From page 38, IS 456

% of steel = 0.66%

$F_s = 0.58 f_y * (A_{streq} / A_{stprov}) = 0.58 * 415 * (1058.6 / 942.47) = 277.24 \text{ N/mm}^2$

From fig 4, IS 456

Modification factor (k) = 1.05

Step 7: Development Length

$(l/d)_{max} = 20k = 20 * 1.05 = 22$

$(l/d)_{prov} = (5000 / 475) = 12.42$

$(l/d)_{max}$  greater than  $(l/d)_{prov}$ , Safe in Deflection.

**Column Design (IS 456:2000)**

Axial load = 2392 KN

Size of column,  $L = 300 \text{ mm}$ ,  $b = 400 \text{ mm}$

**Step1: % of Steel**

$P_t$  greater than 0.8%,  $P_t$  less than 6%

Assuming % = 1.0

$A_{sc} = 0.01 A_g$

$A_c = A_g - A_{sc} = A_g - 0.01 A_g = 0.99 A_g$

**Step2: Depth Required**

$P_u = 0.4 f_{ck} A_c + 0.67 f_y A_{sc}$

$2392 * 10^3 = 0.4 * 25 * 0.99 A_g + 0.67 * 415 * 0.01 A_g$

$A_g = 188636.09 \text{ mm}^2$

$D = (188636.09 / 400) = 471.59$

Provide  $D = 480 \text{ mm}$

Provide  $A_g = 192000 \text{ mm}^2$

**Step3: Check for eccentricity and Slenderness ratio**

$e_{min} = (L / 500) + (D / 30) = (3000 / 500) + (600 / 30) = 26 \text{ mm}$

$e_{min}$  greater than 20

$e_{max} = 0.05 D = 0.05 * 480 = 24 \text{ mm}$

$e_{min}$  less than  $e_{max}$ , ok

Effective length / least lateral dimension =  $3000 / 400 = 7.5$  less than 12

Hence, it is a short column

**Step4: Area of steel**

$2392 * 10^3 = 0.4 * 25 * 0.99 * 192000 + 0.6 * 415 * A_{sc}$

$A_{sc} = 1972.69 \text{ mm}^2$

Use 16 mm dia bars, No of bars =  $(1972.69 / (\pi / 4) * 16^2) = 9.81 = 12$  bars

### Step5: Design of Lateral Ties

Dia of lateral ties not less than  $(1/4) \times \text{dia of reinforcement} = (1/4) \times 16 = 4 \text{ mm}$

But not less than 6mm

Then provide 6mm dia of lateral ties

Spacing not greater than  $b = 400 \text{ mm}$

$16 \times 16 = 256 \text{ mm}$

300mm

Provide 6mm dia, 256 mm spacing of lateral ties

Slab Design (IS 456)

### Step1.

$L_x = 4 \text{ m}$ ,  $L_y = 5.5 \text{ m}$ .

$L_y / L_x = 1.37$  less than 2.

Hence, it is two-way slab.

Live load =  $2 \text{ KN/m}^2$

$f_{ck} = 25 \text{ N/mm}^2$ ,  $f_y = 415 \text{ N/mm}^2$ ,  $b(\text{width}) = 1000 \text{ mm}$

### Step2. Estimations of slab thickness

As  $l_x$  greater than 3.5, Hence  $(l/d)$  is assumed as same for one way slab.

$(l/d) = 25$

Effective depth  $(d) = 4000 / 25 = 160 \text{ mm}$

Over all depth  $(D) = 160 + 25 = 185 \text{ mm}$

### Step3: Effective length

$L_{eff} = 4 + 0.16 = 4.16 \text{ m}$

### Step4: Selfweight

Self weight of the slab =  $D \times 25 = 185 \times 25 = 4.625 \text{ KN/m}^2$

Live load =  $2 \text{ KN/m}^2$

Floor finish =  $1 \text{ KN/m}^2$

Total load =  $7.625 \text{ KN/m}^2$

$W_u = 1.57 \times 7.625 = 11.43 \text{ KN/m}^2$

### Step5: Calculation of ultimate moment

From table 26, IS 456  $\alpha_x = 0.083$ ,  $\alpha_y = 0.056$

$M_x = \alpha_x \times W_u \times L_{eff}^2 = 0.083 \times 11.43 \times 4.16^2 = 16.41 \text{ KNm}$

$M_y = \alpha_y \times W_u \times L_{eff}^2 = 0.056 \times 11.43 \times 4.16^2 = 11.07 \text{ KNm}$

$V_u = (W_u \times L_{eff}) / 2 = (11.43 \times 4.16) / 2 = 23.77 \text{ KN}$

### Step6: Check for depth

$M_{lim} = 0.138 f_{ck} b d^2$

$M_{lim}$  is maximum of  $M_x$  and  $M_y = 16.41 \text{ KNm}$

$16.41 \times 10^6 = 0.138 \times 25 \times 1000 \times d^2$

$d = 68.96 \text{ mm}$  less than  $d_{prov}$

### Step7: Calculation of reinforcement

$M_u = 0.87 \times f_y \times A_{st} \times d \times (1 - (f_y A_{st}) / (f_{ck} b d))$

$16.41 \times 10^6 = 0.87 \times 415 \times A_{st} \times 160 (1 - (415 A_{st}) / (25 \times 1000 \times 160))$

$A_{st} = 292.97 \text{ mm}^2$

Adopt 10mm dia, Spacing =  $(\text{ast}1000 / A_{st}) = ((\pi/4) \times 10^2 \times 1000 / 292.97) = 268 \text{ mm}$

Provide 10 mm diameter @ 268 mm c/c spacing as main reinforcement

### Step8: Calculation of distribution Reinforcement

$M_u = 11.04 \text{ KNm}$ ,  $d = 150 \text{ mm}$  (160-10)

$11.04 \times 10^6 = 0.87 \times 415 \times A_{st} \times 150 (1 - (415 A_{st}) / (25 \times 1000 \times 150))$

$A_{st} = 208.66 \text{ mm}^2$

Assume 8mm dia, spacing =  $((\pi/4) \times 8^2 \times 1000 / 208.66) = 240 \text{ mm}$

Provide 8mm diameter @ 240mm c/c spacing as distribution reinforcement.

**Step9: Check for Shear**

$T_v = (V_u / bd) = (23.77 * 10^3 / 1000 * 160) = 0.14 \text{ N/mm}^2$   
 $T_c, P_t = 100 A_{st} / bd = (100 * 292.97) / 1000 * 160 = 0.18$  and M25 grade  
 $T_c = 0.31 \text{ N/mm}^2$

$T_v$  less than  $T_c$ , Hence satisfied the criteria.

**Step10: Check for Deflection**

$(l/d)_{prov} = (4160 / 160) = 26$   
 $(l/d)_{permitted} = (l/d)_{basic} * k * t = 20kt$   
 $Kt = f_s = 0.58 f_y (A_{streq} / A_{stprov}) = 0.58 * 415 * (292.97 / 314.15) = 224.47 \text{ N/mm}^2$   
 $Kt = 2.0$   
 $(l/d)_{permitted} = 20 * 2.0 = 40$   
 $(l/d)_{permitted}$  greater than  $(l/d)_{prov}$

**Step11: Calculation of reinforcement in edge strip**

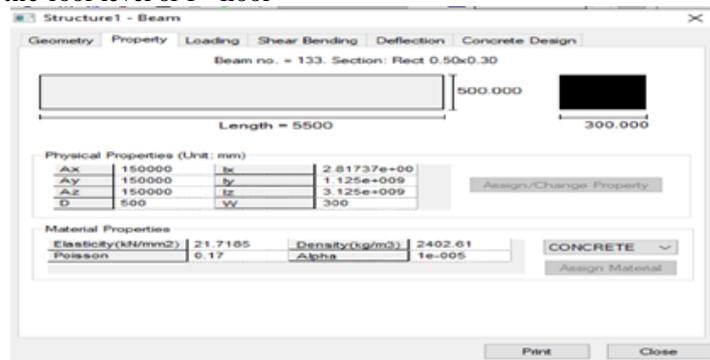
$A_{st\ prov} = (0.12 / 100) * 1000 * 185 = 222 \text{ mm}^2$   
 Assume 6mm dia meter, spacing =  $(ast1000) / A_{st} = (\pi * 6^2 * 1000 / 4) / 222 = 230 \text{ mm}$   
 Provide 6mm dia @ 230mm/c in edge strip.

**Step12: Torsion steel at the corner**

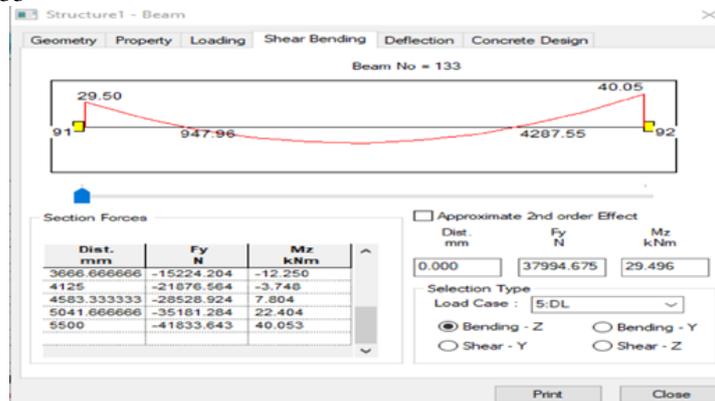
Area of reinforcement to be provided =  $(3/4) * A_{st} = (3/4) * 292.97 = 219.20 \text{ mm}^2$   
 Distance up to which torsion reinforcement is to be provided  
 $(l_x / 5) = (4000 / 5) = 800 \text{ mm}$   
 Assume 6mm dia bars,  
 Spacing =  $((ast * 1000) / A_{st}) = ((\pi / 4) * 6^2 * 1000) / 292.27 = 96.7 = 100 \text{ mm}$   
 Provide 6mm dia @ 100 mm c/c in both the direction at a distance of 800 mm @ 4 Corners.

**Analysis Results**

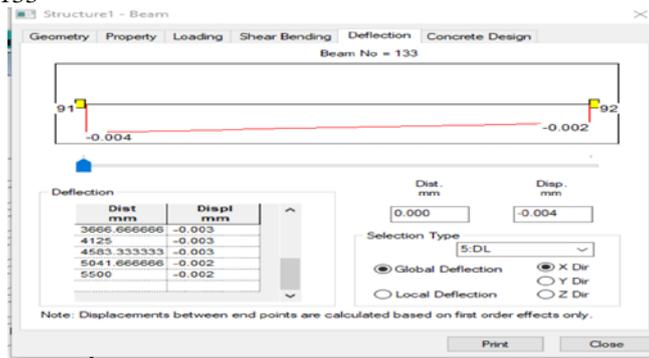
Some of the sample analysis results have been shown below for beam Number 64 which is at the roof level of 1<sup>st</sup> floor



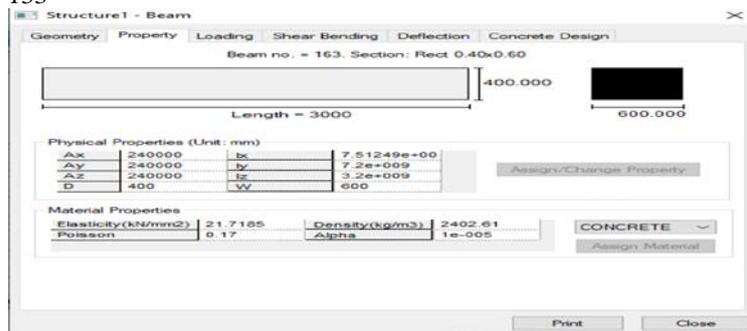
Property of beam no-133



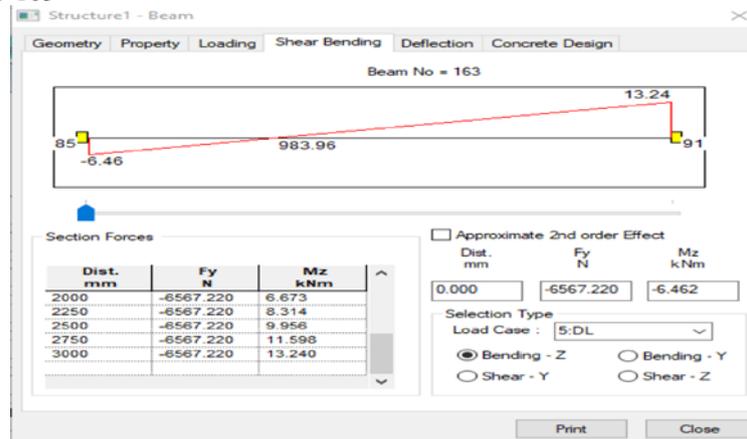
Shear bending of beam no-133



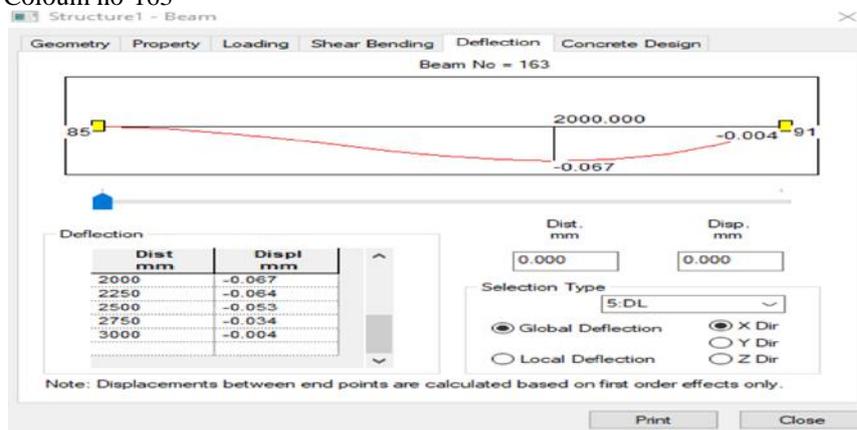
Deflection of beam no-133



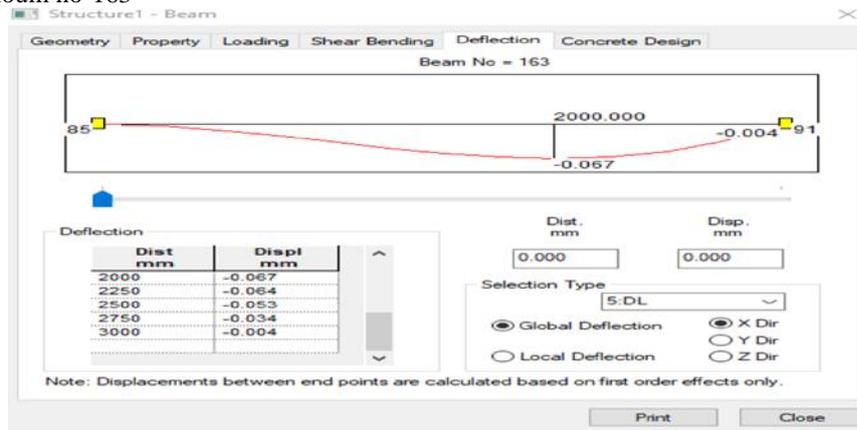
Property of Coloum no-163



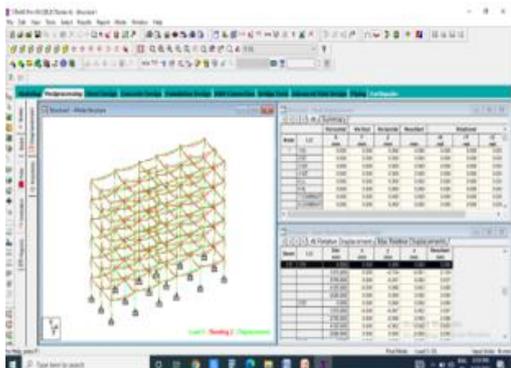
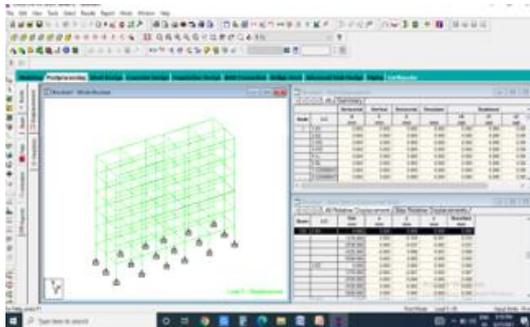
Shear bending of Coloum no-163



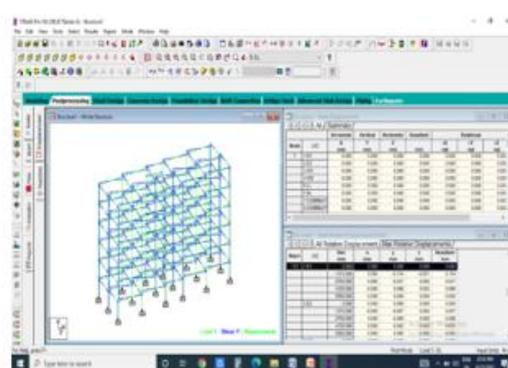
Deflection of Coloum no-163



POST PROCESSING MODE



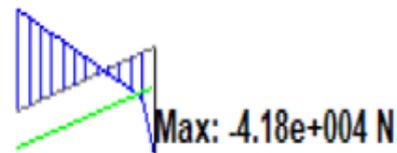
Bending in Z



Bending in Y



Bending moment diagram



Shear force diagram

## V. Results & Discussion

BEAMNO.133 DESIGN RESULTS

M25 Fe415 (Main)Fe415(Sec.)

LENGTH:5500.0mm SIZE:500.0mmX300.0mm COVER:25.0mm

**Summary of Reinforcement Area (Sq.m m)**

**Table5.1: Summary of Reinforcement beamno.133**

Section	0.0mm	1375.0mm	2750.0mm	4125.0mm	5500.0mm
TOPREINF.	286.95(sqmm)	286.95(sqmm)	286.95(sqmm)	286.95(sqmm)	535.43(sqmm)
BOTREINF	286.95(sqmm)	286.95(sqmm)	286.95(sqmm)	286.95(sqmm)	286.95(sqmm)

**Summary of Provided Reinforcement Area (Sq.m m)**

**Table5.2: Summary of Provided Reinforcement beamno.133**

Section	0.0mm	1375.0mm	2750.0mm	4125.0mm	5500.0mm
Toprein.	3-16i2layers(s)	3-16i1layers(s)	3-16i1layers(s)	3-16i1layers(s)	3-16i2layers(s)
Botrein	3-16i2layers(s)	3-16i1layers(s)	3-16i2layers(s)	3-16i1layers(s)	3-16i2layers(s)
Shear rein	2leg12i@170mmc/ c				

**Shear Design Results at Distance D (Effective Depth) from Face of the Support**

Shear Design Results at 665.0 mm away from STRAT SUPPOTS

VY= 41.27MX= 0.30LD= 9

Provide 2 legged 12i@170mmc/ c

Shear Design Results at 665.0 mm away from END SUPPOTS

VY= -56.55MX= 0.35LD= 10

Provide 2 legged 12i@170mmc/ c

**Column No.163 Design Results**

M20Fe415(Main) Fe415(Sec.)

LENGTH:3000mm CROSS SECTION:600.0mmX400.0mmCOVER:40.0mm

\*\*GUIDING LOAD CASE:1 END JOINT:85 SHORT COLUMN

REQD.STEEL AREA:1920Sq.mm.

REQD.CONCRETE AREA:238080Sq.mm.

MAIN REINFORCEMENT:Provide12-16dia.(1.01%,2412.74Sq.mm.)

(Equally distributed)

TIE REIN FORCEMENT:Provide 12mm dia.rectangular ties @225mmc/ c

SECTION CAPACITY BASED ON REINFORCEMENT REQUIRED(KNS-MET)

Puz:3276.00Muz1:107.30Muy1:169.13 INTERACTION RATIO:0.20(asperCl.39.6, IS456:2000)

SECTION CAPACITY BASED ON REINFORCEMENT PROVIDED(KNS-MET)

WORST LOADCASE:1

END JOINT:85Puz:3423.82Muz:133.16Muy:212.46IR:0.16

**Element Design Summary**

ELEMENT LONG.REINF MOM-X/ LOAD TRANS.REINF MOM-Y/ LOAD

(SQ.MM/ ME)(KN-M/ M)(SQ.MM/ ME)(KN-M/ M)

286TOP:126.017/ 10126.011/ 10

BOTT:126.000/ 2126.000/ 3

287TOP:126.014/ 9126.010/ 9

BOTT:126.-0.03/ 1126.000/ 1

288TOP:126.000/ 3126.07/ 10

BOTT:126.-0.26/ 10126.-0.04/ 2

289TOP:126.016/ 10126.010/ 10

BOTT:126.000/ 2126.000/ 4

290TOP:126.013/ 9126.009/ 9

BOTT:126.-0.03/ 1126.000/ 1

291TOP:126.000/ 0126.007/ 9

BOTT:126.-0.23/ 10126.-0.05/ 2

292TOP:126.016/ 10126.010/ 10

BOTT:126.000/ 2126.000/ 3

**VI. Conclusions**

- 1.By Using STADDPro.,analysis and design of multi-storey building is easier and quick process than manual process.
- 2.Proposed size of the beam and coloumn can be safelyused in the structure.

- 3.The structure is safe in shear bending and deflection.
- 4.There is no hazardous effect on the structure due to wind load and seismic load on the structure.
- 5.The structure we taken is stable and structurally defined using various loads and combination.
- 6.The deflection value is more in WL(WindLoad)combination than the SL (Seismic Load) combination.
- 7.To know the behaviour of the structure bya applying various loads like dead load, live load, wind load and seismic load byusing staad.pro.And also find out the Shear forces, displacement, bending and reactions of structure.
- 8.By using staadpro,we performed dynamic analysis.So that,the results obtained in Staad pro is more effective as compared to analysis and design performed by theoretical method.

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