

“Use Of Reclaimed Asphalt Pavement (RAP) Materials In WMM And DBM Layers Of Flexible Pavements”

Harish Kumar Rai

Master Of Technology In Highway Engineering
School Of Engineering And Technology,
Shri Venkateshwara University, U.P.
Gajraula -244236
2025

Abstract

Reclaimed Asphalt Pavement (RAP) is the term to removal and processed materials containing asphalt and aggregate. These materials are generated when asphalt pavement is removed for construction, resurfacing or to obtain excess to buried utilities. RAP material makes both environmental and economic sense. The use of recycle asphalt pavement has grown widely reducing the use of virgin material. When properly crushed and screened, RAP consists of high quality, well-graded aggregate coated by asphalt cement.

A good road network is key for economic and social development of a country. There is about 4.2-million-kilometer road network in India which rank second in the world only after United States. It is necessary to maintain previously constructed roads along with new road construction. Both construction and maintenance of roads leading to over exploitation of resources of aggregates. Most of Indian roads are bituminous surfaced pavements. A good road network is key for economic and social. Apart from depleting resources and Environmental issues, these roads are periodically resurfaced as maintenance action which intend to roads to attain a higher raised level as compared to initial level of road and joining properties and structures level. Recycled or Reclaimed Asphalt Pavement (RAP) has increasingly been used to replace fresh or virgin materials for highway construction and maintenance as an Ecofriendly-Sustainable solution to overcome these problems. RAP can be used in different layers of Flexible and Rigid pavements. In this research paper, an effort has been made to characterize the RAP based on gradation characteristics of RAP aggregate sand sources of RAP.

The use of recycled materials as a sustainable alternative is gaining significant worldwide attention. To achieve the objectives of the research, six proportions of RAP aggregate materials in addition to Virgin Aggregates (VA) were used as categorized below:

Category1: 00% RAP (95%VA+05%Stone dust)

Category2: 10% RAP (75%VA+15%Stone dust)

Category3: 25% RAP (58%VA+17%Stone dust)

Category4: 35% RAP (40%VA+25%Stone dust)

Category5: 45%RAP (25%VA+ 30%Stone dust)

Category6: 60% RAP (05%VA+35%Stone dust)

Use of RAP aggregates along with the new/fresh aggregates will reduce the use of new material for construction of flexible pavement. Also, it will cut down the cost of construction.

Date of Submission: 28-03-2025

Date of Acceptance: 08-04-2025

I. Introduction

Reclaimed asphalt pavement (RAP) is a valuable, high-quality material that can be replace over expensive virgin aggregates and binder that can be used for technical, economic, and environmental reasons.

Large quantities of Reclaimed asphalt pavement (RAP) materials are produced during highway maintenance and construction. A part of this can be used in new hot mix asphalt concrete and rest is available for other uses. If these materials could be re-used in base and sub-base of the roads or also in surface course (for low volume traffic, or in service road), resulting in minimization of environmental impact, reduce the waste stream and transportation costs connected with road maintenance and construction activities.

The properties of RAP materials can be improved by blending of aggregates and by addition of chemical stabilizers. In recent years there was a gradual increase in construction and demolition wastes. It has resulted in waste disposal problem due to shortage of available land fills. Reuse of these material safter proper recycling can be the right solution for the same. There will be a reduction in cost about 25 to 30% by reusing the recycled road aggregate generated at same site. Before using such materials, the mechanical properties must

be tested, and suitable blending is done if required.

The most used recycled materials are Reclaimed asphalt pavement (RAP) materials and recycled concrete aggregate (RCA). The generation of RAP and RCA result in an aggregate of high quality and grading. Due to coating of asphalt on the aggregate of RAP it reduces the water absorption in aggregates. Production of Reclaimed asphalt pavement (RAP) materials:

Removal and reuse of asphalt layer of existing pavement is termed as RAP. However full depth reclamation (FDR) is defined as removal and reuse of hot mix asphalt layer and entire base course. RAP can be reused immediately at sites; however, it may be stockpiled. The required gradation of RAP is achieved by pulverizing the material in a crusher.

A condition of demolished flexible pavement is shown in Fig-1 which can be reused after proper processing and crushed to required size and grading as per requirements of site condition.



Fig.1.1 Dismantling of DBM Layer of Road Surface

Pavements are designed to provide durable all-weather travelling surfaces for safe, smooth and speedy movement of vehicles carrying people and goods with areas on able level of comfort to its users. Road pavements are valuable assets as they constitute primary means of communication and transportation of people, goods and services on a daily basis. The design and construction of pavements requires a fundamental understanding of materials as once they are open to traffic loads, the pavements gradually deteriorate with time, traffic load applications and change in climatic conditions. Lack of maintenance on the pavement could result in rutting, fatigue cracking and other distress types that eventually result in an unacceptable ride quality for users.

Properties of RAP:

A Comparison can be made between RAP and crushed natural aggregates. RAP has a higher content of fines because of degradation of material during milling and crushing operations. Typical physical properties of RAP are tabled below:

Table-1.1. Typical properties of RAP

S. No.	Parameters	Values
1	Unit Weight(Kg/m ³)	1900-2250
2	Moisture Content	Max 3%
3	Asphalt Content	Max 4%
4	Asphalt Penetration(%)at25°C	10-80
5	Compacted Unit Weight(Kg/m ³)	1500-1950
6	California Bearing Ratio(CBR)	100%RAP:20-25%

Consumption of natural aggregate can be reduced by using Reclaimed asphalt pavement(RAP) materials. Amount of binder can also be reduced in asphalt paving mixes by using Reclaimed asphalt pavement (RAP) materials. Studies have revealed that performance of pavement by using up to 30% RAP material is like that of pavement constructed with natural aggregates without RAP materials. Increase demand of aggregates and binder supply can be meet out up to certain extent by using Reclaimed asphalt pavement (RAP) materials in hot mix asphalt (HMA) and other courses of the flexible pavements like sub-base and base. Finally recycling asphalt creates a cycle of reuse that optimizes the use of natural resources and sustains the asphalt industry.

Economy, ecology, and energy conservation are all achieved when the two main components i.e., asphalt and aggregate are reused as construction materials to provide a strengthened and improved pavement.

The use of RAP has become relatively common practice in most countries, as it is both an environmentally and economically attractive proposition. RAP material is generated when old, damaged pavement materials are milled and crushed for addition as a component to new mixtures placed in the pavement structure. Historically, old pavement material was removed and disposed of in landfills.

Methods of Reclaimed Asphalt Pavements

There are several methods of reclaimed asphalt pavements such as:-

- Hot mix plant recycling
- Hot in place recycling
- Cold mix plant recycling
- Cold in place recycling

The addition of Reclaimed asphalt pavement to an asphalt mixture changes the mechanistic property (i.e., strength durability of the mixture and affects its performance).

Hot Mix Plant Recycling

Hot mix recycling is defined as a process that combines RAP with virg in aggregates, bitumen and sometimes recycling agents to produce hot mix asphalt. The RAP may be obtained by pavement milling with a rotary drum, cold milling machine or from a ripping/crushing operation stated that hot mix recycling is the most common method of recycling asphalt pavements and can perform as well as mixtures with entirely new materials.



Fig.-1.2 Hot Mix Plant in Patna-Dobhi Road Project

Hot in Place Recycling

Initially the pavement intended to be recycled is heated to a higher temperature using suitable heating arrangement. This facilitates easier removal of materials. After heating, the pavement surface is scarified to there quired depth. Further, depending on there requirement fresh aggregate and binder are added. The material is mixed well and compacted to there quired thickness. As this process consumes less time, least disruption to traffic is caused. Also, the transportation cost is less, as materials need not be taken away. Machinery required for this purpose being bulky in nature, sufficient right-of-way is required. This becomes an important consideration for in-place recycling within the city areas.

Cold Mix Plant Recycling

Cold mix recycling is a process of recycling without the use of heat where existing asphalt pavements are pulverized, mixed with new virg in aggregates and stabilizing agents to produce a new material that is expected to meet the standards. Cold recycling is an economical technique since the material does not need to be heated contributing to a reduction in energy, fuel, and material consumption.

Cold in Place Recycling

Cold in-place recycling is are habilitation technique where existing asphalt pavement materials are reused and mixed in-place without the application of heat. The RAP is obtained by milling or crushing the existing pavement. Virg in aggregate, recycling agents or both are usually added to the RAP which is then laid and compacted. The use of cold in-place recycling can restore old pavement to the desired profile, eliminate

existing wheel ruts, potholes, irregularities, and rough areas. It can also eliminate transverse, reflective, and longitudinal cracks. This method for the maintenance and rehabilitation of pavements promotes sustainability and helps in limiting the use of scarce materials that include gravel and crushed rock. Cold in-place recycling promotes a high production rate of asphalt mixtures resulting in cost savings, minimum traffic disruption, ability to retain original profile and environmental benefits all without the use of heat.

Need of Study

Reclaimed asphalt pavement (RAP) is the term given to removed and/or reprocessed pavement materials containing aggregates asphalt and. These materials are generated when asphalt pavements are removed for reconstruction, resurfacing or to obtain access to buried utilities. When properly crushed and screened, RAP consists of high-quality, well-graded aggregates coated by asphalt cement. Asphalt pavement is generally removed either by milling or full- depth removal. Milling entails removal of the pavement surface using a milling machine, which can remove up to 150 mm thickness in a single pass and transported to a central facility for processing. At this facility, the RAP is processed using a series of operations, including crushing, screening, conveying, and stacking. RAP can be used to a larger extent as a base course; however, a limitation of using RAP as fill material is the unknown risk of leaching of pollutants from the aggregate to the environment.

RAP can be used as an aggregate substitute material, but in this application, it also provides additional asphalt cement binder, thereby reducing the demand for asphalt cement in new or recycled asphalt mixes containing RAP. As far as life cycle assessment of RAP is concerned, the life of the recycled pavement materials starts at breaking up the existing old pavement, followed by transportation to depositor asphalt/concrete plant, and then followed by crushing, mixing of new pavement material and transportation to the location of the new pavement. In summary, the benefits of RAP include Reduction in CO₂emissions due to lower demand of construction materials, Reduction in the asphalt (bitumen) content, Reduction in the overall cost, almost same if not more of the performance and durability characteristics of a conventional dense graded asphalt concrete materials Cost is an important factor in terms of recyclability and reuse of material and can be an incentive to use such material.

The construction industry will certainly recognize the economic benefits of using recycled materials, such as crushed RAP aggregates for base courses of the pavements. The cost- effectiveness of substituting conventional aggregate with recycled materials is highly dependent on the location, the quality, and cost of local aggregates. Recycling versus tipping fee sand distances to land fills are other important aspects for the feasibility of recycling. In some urban areas recycling can be more profitable than in rural areas. In rural areas recycling can be expensive and impractical due to high transportation cost and the lack of nearby materials. On the other hand, if materials are available, reuse of materials that otherwise have to be transported can be very cost effective. Overall, there is a critical need to understand the use of recycling of existing damaged asphalt pavement materials to produce new pavements with considerable savings in materials, energy, and cost in the Indian context. In addition, aggregate sand binders from old asphalt pavement are still valuable even though the damaged pavements have reached the end of their service lives.

- The demand of aggregate to construct pavement is more & more so to recover it and for the optimization of natural resources.
- To overcome the problem related to dumped materials and recycle of dumped material and conserve the natural resources.
- To minimize the adverse effect on environment.
- To use the Recycled material as filling material without doing any analyzed and test in low lying areas.
- To use the Recycled material as WMM after investigating and then adding them is single sieve size material.

Aim

Proposing use of Reclaimed Asphalt Pavement (RAP) in WMM layer and DBM layer of flexible pavement.

Objective

The main objective of the study is to develop specifications and practices for recycled asphalt pavement (RAP) mixes and to understand the performance characteristics of the asphalt mixes, mainly from the perspectives of materials, energy, and costs. The proposed work envisages the following scope of the effort:

- Review of the RAP mix design methods practiced worldwide.
- Select appropriate percentage of RAP to be used with new materials which will result in adequate density (and porosity) of the conventional mixes.
- Investigate the use of modifiers (crumb rubber and polymer additives) in the RAP mix designs.
- Conduct material characterization (binder sand mixtures) laboratory test to evaluate for their rutting, cracking, and moisture resistance characteristics.

- Compare the test results with the performance of the traditional control conventional asphalt mixes in the laboratory with the RAP (conventional and modified) mixes.
- Develop rutting, cracking and moisture performance criteria and models.
- To reduce the use of fresh aggregates up to the possible extent.

Scope & Limitation

The scope of my study is as follow: -

- To carry out detailed study of literature and pavement construction practices.
- Use of RAP material in flexible pavement.
- Review on foam and emulsion based cold recycle asphalt mixes
- To carry out various laboratory teston material sand RAP

The limitation of my study is as follow:

- Hot mix plant recycling method is used for laboratory tests to calculate the various engineering property of reclaimed asphalt pavement.
- All the results of various laboratory test on material and RAP are compared with IS codes and MoRTH guidelines of pavement design

Methodology

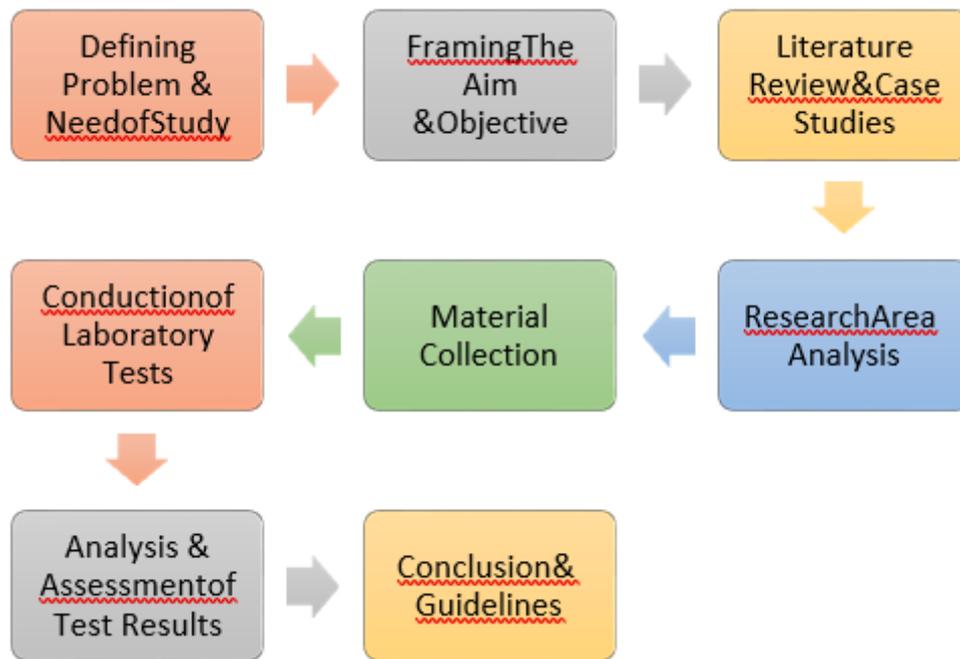


Fig 1.3-methodology

Report Structure

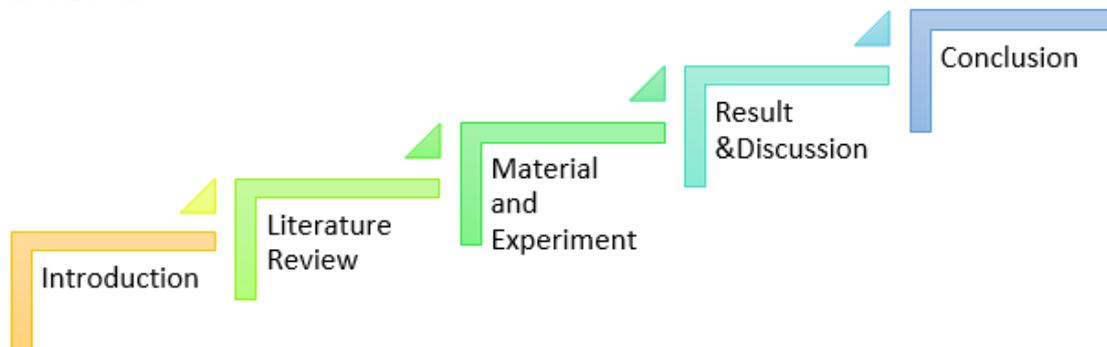


Fig-1.4

II. Literature Review

The present investigation deals with studies & ground implementation on the mix design of emulsion treated reclaimed asphalt pavement and so an attempt has been made to briefly review the available literature on the following topics:

Evaluate the amount of blending that occurs between RAP and virgin asphalt binders in plant produced HMA in which RAP is incorporated.

- Review On Foam and Emulsion Based Cold Recycled Asphalt Mixes.
- Case Study on Cement Treated Rap Containing Asphalt Emulsion and Acryl Polymer: Many research and investigations were conducted on cold and hot mixes of RAP all over the world. Some reviews on recycled material mix are as follows.

Many research and tests were conducted on cold and hot mixes of RAP all over the world. Some reviews of mix design are as follows:

Evaluation of Blending that Occurs between RAP and Virgin Asphalt Binders by L.Allen Cooley, Jr., Ph.D. Kevin Williams, P.E

{The objective of this study was to evaluate the amount of blending that occurs between RAP and virgin asphalt binders in plant produced HMA in which RAP is incorporated. Recycled Asphalt Pavement (RAP) is the most recycled material in the U.S.R A P has been routinely used in the production of hot mix asphalt (HMA) since the 1970's. Historically, there have been three theories of how RAP behaves when included within HMA. The first is that the highly oxidized asphalt binder contained within the RAP essentially makes the RAP a “black rock”. The second theory is that the asphalt binder within the RAP becomes fluid during the production and construction process and totally blends with the new, virgin asphalt binder. In 2011, the Federal Highway Administration (FHWA) estimated that over 90 percent of the highway and roads with in the US were constructed with hot mix asphalt (Copeland,2011). As these pavements age and fulfill their intended performance life, there will always be a need to maintain, rehabilitate, or reconstruct these pavements. In many instances, cold planning is used to remove a layer of HMA that has become distressed. Cold planning is the removal of an existing pavement to a desired depth. After an asphalt pavement has been removed, one option is to recycle the material back into an HMA in the form of recycled asphalt pavement (RAP). As described in the FHWA quote, there cycling of HMA pavement scan provide economic and environmental benefits. Copeland (2011) stated that RAP is a useful alternative to virgin aggregates during the production of HMA. The use of RAP minimizes the tonnage of virgin aggregates that must be bought. Copeland (2011) also states that the amount of virgin asphalt binder that must be purchased is reduced. Both virgin aggregates and virgin asphalt binder are non-renewable resources, so the use of RAP also provides an environmental benefit.

The objective of this study was accomplished by testing plant produced mixture from three different on-going HMA projects. Two of the three projects incorporated 15 percent RAP within the HMA while the third project incorporated 30 percent. Samples were obtained at three locations during the production and construction process. These samples were brought back to the laboratory and subjected to a staged extraction/recovery process. Based upon the research approach for this project, the following conclusions are provided.

- Asphalt binder content measurements for HMA determined using the ignition oven are generally higher than asphalt binder contents determined using solvent extraction.
- The difference in measured asphalt contents between the ignition oven and solvent extraction appear to be aggregate type dependent.
- Failure temperatures measured using the DSR were relatively consistent within each stage for mixes containing 15 percent RAP.
- Failure temperatures measured using the DSR were higher for mixes containing 30 percent RAP.
- The stiffness of the blended asphalt binder generally increased for each stage for all mixes containing RAP. The asphalt binder recovered in each stage for the 30 percent RAP mixes increased at a greater rate than mixes containing 15 percent RAP.
- For mixes containing 30 percent RAP, most of the asphalt binder within the mix was not significantly affected by the aged RAP asphalt binder. The RAP asphalt binders significantly affected 5 to 13 percent of the total asphalt binder extracted. Another 18 percent was affected; however, the failure temperature was like a PG76-XX asphalt binder.
- The theories of RAP behaving as a black rock and total blending of RAP and virgin asphalt binders were proven false. The data explicitly shows that partial blending takes place between RAP and virgin asphalt binders.

Review on Foam and Emulsion Based Cold Recycled Asphalt Mixes by Siksha Swaroopa Kar, Arvind Krishna Swamy, Devesh Tiwari, Dr. P. K. Jain

Due to the increase of road infrastructure around the world, its impact on the environment and scarcity of aggregates requires serious attention to construction of sustainable pavement which constitutes towards the use of cold mix recycled asphalt technology. Cold mix recycled asphalt with bitumen emulsion and Foamed bitumen is a technique still in development, which has proved to be very promising, both in economic and environmental terms. This technology saves energy, natural resources, reduces CO emissions as recycling is done at lower temperature and increases the number of recycled materials. The objective of this review is to summarize the study on Foam Bitumen and Emulsion incorporating RAP in construction materials, which is a challenging task due to the heterogeneity of the materials. Conservation of energy and materials is important practices for achieving sustainability in road construction. Major road infrastructure activities currently under taken by different agencies for the last one decade have shown greater impact on energy consumption and depletion of aggregates. The production of huge quantities of Hot Mix Asphalt (HMA) releases a significant amount of greenhouse gases. Also, there is a problem of the scarcity of aggregates and aggregate being very expensive because of large lead distances, therefore, a serious attempt must be made to develop and adopt alternative technologies for road construction and maintenance to reduce consumption of fuel and aggregates. It is also to be noted that thicknesses of existing pavements are increasing due to addition of periodic overlays.

The rise of road levels causes serious drainage problems in the urban areas. In such cases, the existing bituminous pavement usually consisting of Dense Bituminous Macadam (DBM) and Bituminous Concrete (BC) can be milled and the Reclaimed Asphalt Pavement (RAP) transported to cold mix plant for recycling on service roads and/or main line. Bituminous pavements are 100% recyclable. Milling of existing pavements and recycling the same after suitable modification will address problems of drainage and conservation of materials. Recycling of existing pavements is a common practice in South Africa, Europe and United States. Use of either hot or cold in-place in-plant techniques to rehabilitate the distressed pavements has been practiced for a long time. The purpose of this State-of-the-Art is to summarize the leading studies including scientific papers, technical reports and thesis that have been conducted on Foam bitumen and Emulsions over the last decade, and to draw general conclusions regarding the present state of knowledge of Cold Recycled Mixes.

Case Study on Cement Treated Rap Containing Asphalt Emulsion and Acryl Polymer By Masoud Faramarzi

A Korean contractor developed and used a cement treated Reclaimed Asphalt Pavement (RAP) containing asphalt emulsion and acryl polymer as base layer in Korea.

Unfortunately, it was reported that the performance of the mixture was controversial by appearance of reflective and other cracking on the surface of the pavement. In the phase one study, main goals were evaluation of some mechanical properties as well as understanding the material category of this mixture. To achieve these goals, a series of literature reviews and laboratory tests were carried out including Marshall stability and flow, indirect tensile strength, water sensitivity, rutting resistance and compressive strength of both “Contractor mix” and Rhode Island (RI) pavement materials i.e., typical hot mix asphalt (HMA) and Portland Cement Concrete (PCC). According to the Asphalt Pavement Analyzer (APA) test results, it was observed that “Contractor mix” behaved like an elastic material at low temperatures while it tends to behave like a visco-elastic material at high temperatures to some extent. Also, it was resistance enough against the moisture damages and rutting phenomena, however, showed considerably lower compressive strength compared to PCC. Because of low compressive strength and probably high shrinkage of this mixture, it could be problematic to use it as base layer material and could affect pavement resistance against some distresses, particularly transverse and reflective cracking. Finally, because of high cement content and rigid behavior it was decided to model this material as concrete and/or cement treated RAP material in the second phase of this study.

For more than a century, Hot Mixed Asphalt (HMA) has been used for paving roads and streets. Since the mid twentieth century, transportation organizations have recycled old broken asphalt mixtures for reuse, instead of disposing the asphalt mixture in landfills. In the 1970's, these organizations recycled more HMA than ever before because oil prices increased and access to high quality aggregates became more difficult. When old or distressed asphalt concrete is recycled, it can qualify for reused in asphalt pavement layers. Recycled Asphalt Pavement (RAP) is generated by milling partial or full depth asphalt pavement scheduled for removal.

RAP must be modified to meet the requirements for the binder and aggregate specifications. First, the asphalt content may not be sufficient for making a new asphalt mixture, and on the other hand, because of exposure to weathering and sun light, the old asphalt binder is usually more brittle than a newer one. Therefore, adding some rejuvenators or additives, e.g., emulsions can compensate for these deficiencies. Secondly, because of milling and crushing operations

during the asphalt pavement removal process, RAP aggregates do not contain enough coarse aggregate. Adding some additional virgin coarse aggregate can not only meet the grading requirements, but also improves the quality of aggregates. Thirdly RAP modifications can be accomplished by the addition of some stabilizer or additives such as Portland cement and Polymeric additives etc.

These materials can change quality of RAP mixture by improving the mechanical properties and decreasing the moisture sensitivity of mixture.

Asphalt emulsion and foamed asphalt are the most common materials used in cold recycling of asphalt pavements. These emulsions which make it feasible to recycle old asphalt concrete at low temperatures at the plant or in place, and these processes are called Cold Central Plant Recycling and Cold In-Place Recycling, respectively. The cold recycling methods lead to more economic, environmental and construction benefits in comparison with hot recycling method. One of additives, which could be added to RAP, is Portland cement. Portland cement looks promising to improve mechanical properties of cold recycled asphalt concrete because of the following reasons:

- Portland cement accelerates curing process of emulsions in cold recycled asphalt mixture.
- Portland cement increases viscosity of binder.
- Portland cement binder probably increases resistance of mixture against compressive stresses in comparison with neat asphalt binder.

However, Portland cement and asphalt emulsion have different basis, and their bond and interactions may lead to deficiencies in the produced mixture. Another issue which could be controversial for this mixture is, understanding its behavior at different temperatures. Pavement designers need to know properties of materials to be able to predict their behavior under different pressures and temperature. Mixture containing both asphalt emulsion and Portland cement could be hard to predict, because Portland cement is an elastic material and its mechanical properties are almost independent to the changes of temperature, while asphalt is a visco-elastic material that its physical and mechanical properties are highly dependent on the temperature.

Much research has been conducted on asphalt emulsion cold recycled mixtures very few studies have been performed on cold recycled mixtures containing high Portland cement. Mixture

evaluated in this study was design about 20 years ago in Korea as a cold central plant recycled asphalt mixture, to be used in the base layer. However, because of too high ratio of cement to emulsion, it became too brittle and more like cement treated RAP mixture.

Unfortunately, it was observed that the pavement with this mixture (“Contractor mix”) had cracks and other distresses on the surface. Because of lack of research and specifications about cold recycled asphalt mixtures at that time, it was not designed according to any confirmed procedure.

That is why researchers in this study were suspicious about this material as a cold recycled asphalt mixture and tried to understand category and characteristics of this material via performing a literature review and experimental investigation.

While initially this material was named cement treated cold recycled asphalt mixture, because of different nature of this mixture compared with cold mix asphalts, it will be called as “Contractor mix” in the rest of this manuscript.

Because the studied material includes both asphalt emulsion and Portland cement it was a kind of new nature, so, not quite the same material could be found at the conducted literature reviews, however, the following studies were found to be the closest ones.

It was observed that some of RAP aggregates were crushed when they were being compacted by Marshall Hammer. It can affect grading of aggregates in “Contractor mix” specimens and consequently may not represent materials in the field. On the other, SGC could better lead to specimens representing “Contractor mix” in the field. Also, it was found that “Contractor mix” specimens had higher Marshall Stability, less flow, and less density in comparison with HMA.

Casestudy on Effect of Water Submergence on the Characteristics of Bituminous Mixes Using Reclaimed Asphalt Pavement by Md. Akhtar Hossain

The main purpose of this study is to investigate the effect of water on the use of reclaimed asphalt pavement materials in bituminous mix and to determine the optimum percentage of reclaimed asphalt pavement materials with virgin pavement materials and optimum days of water submergence according to the Marshall Mix design criteria based on medium traffic condition. To achieve the objectives of this study the basic property tests were performed on the studied materials and then Marshall Test was conducted on asphalt mixtures with different percentages of reclaimed asphalt pavement materials with optimum bitumen content

determined for 100% fresh aggregate. The different percentages of reclaimed asphalt pavement material in asphalt mixtures are 0%, 10%, 20%, 30% and 40%. Marshall Criteria was satisfied up to 20%. Then the

specimen prepared with 20% reclaimed asphalt pavement material was submerged in water at 0, 5, 10, 15 and 20 days. Optimum days of water submergence were 15 days on the basis of Marshall Mix design criteria.

Case study on Use of Reclaimed Asphalt Pavement (RAP) Materials in Flexible Pavements by Brajesh Mishra

In this study sample of Reclaimed asphalt pavement (RAP) materials were collected and analyzed for suitability of their usage in flexible pavements. Their characteristics including gradation, California Bearing Ratio (C.B. R). Aggregate Impact value, Aggregate Crushing value, Specific gravity, Flakiness & Elongation Index, Loss Angles Abrasion value, Water absorption and soundness were determined and compared to the MORTH specifications. From the study it was found that the RAP materials can be effectively used in the soil subgrade, sub-base and base of the flexible pavements resulting in reduction of the construction cost. The main objective of the study is to find out suitability of Reclaimed asphalt pavement (RAP) materials to be used in construction of flexible pavements. To perform experimental investigations to assess the values of related parameters and their technical viability.

Stated the Performance Evaluation of Warm Mix Asphalt Mixtures with Recycled Asphalt Pavement by Burak Sengoz

This paper shows the feasibility of utilizing four different WMA additives (organic, chemical, synthetic zeolite, and natural zeolite) with different rates of RAP. Following the determination of optimum RAP content corresponding to each WMA additive, Marshall Analysis, indirect tensile stiffness modulus and fatigue behavior of HMA and WMA involving RAP were analyzed and compared with control specimens. Hamburg wheel tracking device was also utilized to evaluate the permanent deformation characteristics of mixtures containing optimum RAP content. In this research, RAP has been used (at contents of 10–50%) within both HMA and WMA mixtures. Each type of WMA mixture has been prepared with an optimum rate of WMA additive that is based on the recommendation of manufacturers (organic additive at a rate of 3%, chemical additive at a rate of 2% and two types of water containing additives at a rate of 5% by weight of the bitumen). The mechanical performances of the samples were evaluated by Marshall Stability test. Following the determination of optimum RAP content regarding each mixture involving four different types of WMA additive, indirect tensile stiffness modulus (ITSM) and fatigue behavior of WMA and HMA containing optimum RAP content were analyzed and compared with control specimens. Hamburg wheel tracking device was also used to determine the rutting properties of mixtures involving optimum RAP content.

Case Study on the utilization of recycled asphalt pavement in the Urban Area at Surat, Gujarat, India by Maulik Rao

The main / primary objective was to justify the cost of milling and to make it viable option so that the same can be used effectively. Some practical options to use the RAP material in urban areas are discussed in this study and thereby achieving economy in the construction besides solving the raised level of roads, effective disposal of RAP and above all using the principles of environment friendly green technology that is: Reduce, Reuse and Recycle. The practical study shows the definite impact on replacement of virgin material for various road constructions. The CBR values increasing to 2%, 3.8% and 6.8% respectively by 20%, 40% and 60% RAP mixing in black cotton soil surely work for improved sub-grade.

Case study on Laboratory investigation of Portland cement concrete containing recycled asphalt pavements by Baoshan Huang, Xiang Shu, Guoqiang Li

In this paper, they used the RAP as aggregate in both fine and coarse, and conducted experimental study on its behavior, how it effects on the properties of the concrete like compression, toughness, etc. in this study they are prepared four concrete mixes with and without RAP the RAP using percentages for mixes are 0% & 0%, 100% & 100%, 100% & 0%, 0% & 100% both coarse RAP and fine RAP respectively in each case. They conducted compression study on RAP concrete with concrete made with rubber aggregates. The rubber is replaced as aggregates with various percentage of volume of aggregates they are 0%, 10%, 15%, 25%, 50%. As the percentage of rubber is increasing in the concrete, in same manner strength of concrete also decreasing. The authors conclude that from investigation result RAP concrete is better than the rubber concrete. The concrete made with one coarse RAP is giving good strength than other. RAP concrete had more toughness than nominal concrete.

Case study on the Performance-Related Tests of Recycled Aggregates for Use in Unbound Pavement Layers by Athar Saeed

This study is performing test on RAP and RCP (reclaimed concrete pavement) these materials are used as aggregates in the unbounded base and subbase pavement layers. He conducted different laboratory test

for selection material and to find properties of material on the RAP and RCP, test like sieve analysis for screening, toughness test, moisture and absorption test, stiffness test and frost susceptibility. The properties of these recycled aggregates adversely affecting the performance of the unbound base and subbase pavements like shear strength, durability, stiffness of layer etc. Whatever the use of recycled aggregate like RAP, RCP etc, in unbound base and subbase pavement layer make project more economical.

2.10 Case study on Concrete Containing RAP for Use in Concrete Pavement by Michael J. Bergin, Mang Tia, and Nabil Hossiney (2010)

In this experiment they had replaced the natural aggregate with the RAP in concrete. The concrete containing RAP in percentages 0, 10, 20, 40 were casted in laboratory and evaluate performance of replaced concrete. The investigation results show that, the RAP is adversely affecting on concrete properties they are compressive & flexural strength, elastic modulus. These properties are decreasing with increasing the percentage of RAP, but it didn't affect the thermal expansion, dry shrinkage of the concrete. The evaluation is carried with software analysis, the analysis was performed on both RAP concrete and normal concrete. The software used for analysis is finite element analysis of concrete slab, of version four (FEACONS IV). This software has developed by university of Florida for transportation department to analyze performance of PCC pavements under load and thermal effect conditions. The analysis says that maximum stress to flexural ratio is decreasing with increasing RAP content.

Learnings from Literature Review

- The main carriage way section of Tumkur–Honnar Highway, NH-206 near Tumkur strength end by Full Depth Reclamation (FDR) Technology with a Commercial Cementitious Stabilizer. The pavement section is able to withstand heavy traffic. FWD tests was done to verify design modulus and GPR test was done to check the uniformity & crack formation in cementitious layer.
- The one side carriage way of Bangalore University in front of Civil Engineering Department was strengthened by Cold Recycling Technology with a Commercial Cementitious Stabilizer. The pavement section is able to withstand heavy traffic in the night-time as the road is connecting two major roads approaching Bangalore city. The stretch was evaluated for roughness & stiffness by MERLIN & Geo-gauge respectively.
- Chennai Tada NH 5 Section total of 12 km with width of 8.75m.
- Baroda Halol phase I total length of 11 km recycled to a depth of 20cm.
- Baroda-Halol (Phase 2) the total section of 6 km was executed to a depth of 16cm with foam bitumen as binder.
- Ahmedabad Mehsana 6 km of cold recycling to a depth of 160mm under rehabilitation by cold recycling using foam bitumen as binder.
- Hot in-situ recycling of Mehrauli to Badarpur under Delhi PWD.
- Recycling of roads in Delhi under Delhi PWD.
- NH-6 in West Bengal: Cold in-situ recycling of Reclaimed Asphalt Pavement was done in 2004 and pavement evaluation before and after the recycling showed marked improvement in the strength of the pavement. Pavement performance is evaluated by FWD and modulus of the RAP improved considerably.
- Plant recycling was done in Kolkata on a heavily trafficked main road (Prince Anwar Shah Road) using foamed bitumen. Pavements were evaluated both before milling the bituminous surface and after the construction of the foamed bituminous base and Semi Dense Carpet wearing course. The road was found to be sound even after the two heavy monsoons along with occasional waterlogging.

The review of literature on earlier works reveal the following:

- Industrial wastes can be consumed as by-products and can specially be used as fine- aggregate and / or micro filler in concrete mixtures, inducing benefits on its mechanical properties.
- Natural wastes like rice husk-ash, coconut fiber, durain fiber, wood sawdust and limestone dust composition produce a comparatively lighter than conventional concrete brick. It does not exhibit a sudden brittle fracture even beyond the failure loads and indicates high energy absorption capacity by allowing laboring cost. Also, its compressive and flexural strength values satisfy the requirements of BS 6073 for a building material to be used in the structural application.
- Also, most of the investigations were carried out on a lot of industrial wastes like fly- ash, boron waste and blast furnace slag as replacement of fine aggregates in concrete blocks. Only very few literature surveys were available in regard to papercrete.
- In the earlier works, attempts have been made by a few authors to investigate the paper mill residuals and waste papers sludge ash on the strength and other engineering properties of concrete or building blocks.
- There is a lot of scope for studying the papercrete bricks and its impact on the various engineering properties.

Current Management Options

Recycling

The majority of the RAP that is produced is recycled and used, although not always in the same year that it is produced. Recycled RAP is almost always returned back into the roadway structure in some form, usually incorporated into asphalt paving by means of hot or cold recycling, but it is also sometimes used as an aggregate in base or subbase construction.

It has been estimated that as much as approximately 33 million metric tons (36 million tons), or 80 to 85 percent of the excess asphalt concrete presently generated, is reportedly being used either as a portion of recycled hot mix asphalt, in cold mixes, or as aggregate in granular or stabilized base materials. (2) Some of the RAP that is not recycled or used during the same construction season that it is generated is stockpiled and is eventually reused.

Disposal

Excess asphalt concrete is disposed of in landfills or sometimes in the right of way. In most situations, this occurs where small quantities are involved, or where the material is commingled with other materials, or facilities are not readily available for collecting and processing the RAP. It is estimated that the amount of excess asphalt concrete that must be disposed is less than 20 percent of the annual amount of RAP that is generated.

Market Sources

In most cases, recycled hot mix asphalt can be obtained from central RAP processing facilities where asphalt pavements are crushed, screened, and stockpiled for use in asphalt concrete production, cold mix, or as a granular or stabilized base material. Most of these processing facilities are located at hot mix asphalt plant sites, where the RAP is either sold or used as feedstock for the production of recycled hot mix asphalt pavement or recycled cold mix.

The properties of RAP are largely dependent on the properties of the constituent materials and asphalt concrete type used in the old pavement. Since RAP may be obtained from any number of old pavement sources, quality can vary. Excess granular material or soils, or even debris, can sometimes be introduced into old pavement stockpiles. The number of times the pavement has been resurfaced, the amount of patching and/or crack sealing, and the possible presence of prior seal coat applications will all have an influence on RAP composition. Quality control is needed to ensure that the processed RAP will be suitable for the prospective application. This is particularly the case with in-place pavement recycling.

Applications

The RAP material replaces the natural aggregate in base layer of flexible pavements, resulting in a saving of construction cost.

Reclaimed asphalt pavement material has the higher content of fines because of degradation of material during milling and crushing operations it can be easily used for soil stabilization purpose to increase the CBR value of subgrade to which the crust thickness of road will be reduced, resulting in reduction of cost of construction.

The RAP material can be successfully used in granular subbase layer of flexible pavement after blending to match the requirement grading as per MORTH & IRC specifications for base & subbase material.

In Full depth reclamation (FDR) all the reclaimed materials of the pavement, with or without fresh materials, is stabilized in-situ with suitable stabilizers to produce the base course of the pavement to be overlaid by bituminous course(s). If economically feasible.

After treating the RAP material with emulsion/foamed bitumen in cold mix technology gives the better serviceability for low volume traffic road (slip service road).

Advantages of Reclaimed Asphalt Pavement Materials:

- All the problem related to disposal of RAP wastes can be easily solved and adverse effect on environment may be avoided by the using the RAP materials in flexible pavements constructions, so it is also an ecofriendly treatment.
- In cold mix plants recycling process we are done by some minor modification in WMM plant by which we can reduce the cost of separate batching plant.
- Saving of bituminous binder content as compared to other conventional bituminous mix because recycled material also acervulinesome bitumen binder which is formed strong bond between RAP material and fresh aggregate in summer vacation.
- Low energy consumption in cold mix process as compared to hot mix technology because in hot mix technology High energy consume for heating the ingredients of mix.

- Reduction in consumption and use of natural resources.
- Reduction in damages to the roads due to transportation of materials from quarry sites.
- Conservation of energy
- Preservation of environment
- Reduced cost of construction.
- Conservation of aggregate and binder
- Preservation of existing pavement geometric etc.

Studies have shown that up to 50% of RAP has been used as a partial replacement of granular sub-base and wet mix macadam (WMM) in various projects of National Highway Development Plan (NHDP) in India. Recycling of milled bituminous material has been gaining popularity in India in recent times due to several successful trials in selected projects. A detailed laboratory investigation is required to use RAP in Hot mix asphalt (HMA) and Cold asphalt mix (CAM) to ensure that mixes have necessary minimum strength and durability. For better performance the following points should also be considered which are listed below:

- Quality control and additional processing
- Classifying RAP
- Changing the virgin binder grade

III. Material & Methodology

The material to be used includes recycled bituminous material, RAP materials, fresh aggregate, cement (filler), Stone Dust, emulsion (binder) and water.

Table 3.1-Source of Materials

SrNo	Types of Materials	Source
1	20 mm	Hunturganj
2	Stone Dust	Rafiganj
3	SS2 Emulsion	Howrah
4	RAP Material	Existing Road Pavements
5	Cement	OPC 43 Ultratech

Aggregates (20mm)

Milling (recycled) material does not have any proper gradation as per my mix design requirements so here we used 20 mm size virgin aggregate for maintaining gradation as per IRC:37-2012 Table no IX-1. Aggregate productions were done on my hunterganj crusher and for testing in laboratory Sample were taken from Dobhi camp stockpile.

Some quality assurance tests were performed on 20 mm down aggregate in site laboratory before using as a ingredients of mix design. Tests were conducted on coarse aggregate like as aggregate impact value test, flakiness indices and elongation indices test, specific gravity and water absorption test and individual gradation.

The aggregates from RAP may not have the required gradation for a good mix and used fresh aggregates in RAP materials.

Some tests are performed on aggregates are:

Aggregate impact value (IS:236,PART4),1963

Flakiness and elongation indices test as per Part I & MORTH

Specific gravity test and Water absorption as per IS2386 Part 3 & MORTH

Aggregate Impact Value Test

Toughness is the property of a material to resist impact. Due to traffic loads, the road stones are subjected to the pounding action or impact and there is possibility of stones breaking into smaller pieces. The road stones should therefore be tough enough to resist fracture under impact. A test designed to evaluate the toughness of stones i.e., the resistance of the fracture under repeated impacts may be called an impact test for road stones. Objective: To determine the toughness of road stone materials by Impact test.

Apparatus:

Impact Testing Machine: The machine consists of a metal base with a plane lower surface supported

well on a firm floor, without rocking. A detachable cylindrical steel cup of internal diameter 102mm and depth 50mm is rigidly fastened centrally to the base plate. A metal hammer of weight between 13.5 and 14.0 kg having the lower end cylindrical in shape, 100mm in diameter and 50mm long, with 2mm chamfer at the lower edge can slide freely between vertical guides and fall concentric over the cup. There is an arrangement for raising the hammer and allowing it to fall freely between vertical guides from a height of 380mm on the test sample in the cup, the height of fall being adjustable up to 5mm. A key is provided for supporting the hammer while fastening or removing the cup.

Measure: A cylindrical metal measure having internal diameter 75mm and depth 50mm for measuring aggregates.

Tamping Rod: A straight metal stamping rod of circular cross section, 10mm in diameter and 230mm long, rounded at one end.

Sieve: IS sieve of sizes 12.5mm, 10mm, and 2.36mm for sieving the aggregates.

Balance: A balance of capacity not less than 500gm to weigh accurate up to 0.1gm.

Oven: A thermostatically controlled drying oven capable of maintaining constant temperature between 100 C to 110 C.



Fig3.1-AIV Machine

Procedure:

The test sample consists of aggregates passing 12.5mm sieve and retained on 10mm sieve and dried in an oven for four hours at a temperature 100C to 110C and cooled. Test aggregates are filled up to about one-third full in the cylindrical measure and tamped 25 times with rounded end of the tamping rod. Further quantity of aggregates is then added up to two-third full in the cylinder and 25 strokes of the tamping rod are given. The measure is now filled with the aggregates to overflow, tamped 25 times. The surplus aggregates are struck off using the tamping rod as straight edge. The net weight of the aggregates in the measure is determined to the nearest gram and this weight of the aggregates is used for carrying out duplicate test on the same material. The impact machine is placed with its bottom plate flat on the floor so that the hammer guide columns are vertical. The cup is fixed firmly in position on the base of the machine and the whole of the test sample from the cylindrical measure is transferred to the cup and compacted by tamping with 25 strokes.

The hammer is raised until its lower face is 380mm above the upper surface of the aggregates in the cup and allowed to fall freely on the aggregates. The test sample is subjected to a total 15 such blows, each being delivered at an interval of not less than one second.

The crushed aggregate is then removed from the cup and the whole of it is sieved on the 2.36mm sieve until no further significant amount passes.



Fig3.2-Passing 12.5mm Sieve



Fig3.3-Tamping on Aggregates

Table 3.2- AIV Test Report

AGGREGATE IMPACT VALUE					
Asper IS 2386-Part IV					
S. No	Determination	Trial I	Trial II	Trial III	Average
1	Total Wt. Of Oven-dried Sample (passing 12.5mm-Retained 10mm Sieve)-W1 [gms]	355	357	350	26.66%
2	Wt. Of Material Retained on 2.36mm after testing-W2 [gms]	280	277	275	
3	Wt. Of Material Passing on 2.36mm after testing-W3 [gms]	75	80	75	
4	Difference in weight after testing (W1-W2-W3)	0.0	0.0	0.0	
5	Aggregate Impact Value (%) = $(W3/W1) \times 100$	21.13	22.41	21.43	

The fraction retained on the sieve is also weighed and if the total weight of the fractions passing and retained on the sieve is added it should not be less than the original weight of the specimen by more than one gram, if the total weight is less than the original by over one gram the results should be discarded, and a fresh test made.



Fig3.4- Sieve with 2.36mm Sieve



Fig3.5- Giving 15 blows by using AIV

The aggregate impact value is expressed as the percentage of the fines formed in terms of the total weight of the sample.

Where, W1= Original weight of the sample.

W2= Weight of fraction passing 2.36mm IS sieve.

Results:

The mean of the three results is reported as the AIV (Aggregate Impact Value) of the specimen to the nearest whole number.

Limits:

<10% Exceptionally strong.

10 – 20% Strong

20 – 30% Satisfactory for road surfacing.

>35% Weak for road surfacing.

Flakiness and elongation indices test. Introduction:

The particle shape of aggregates is determined by the percentages of flaky and elongated particles contained in it. For base course and construction of bituminous and cement concrete types, the presence of flaky and elongated particles is considered undesirable as they may cause inherent weakness with possibilities of breaking down under heavy loads. The angularity number i.e., flakiness and elongation has considerable importance in the gradation requirements of various types of mixes such as bituminous concrete,

cement concrete and soil aggregate mixes.



Fig3.6- Sieve Used in Flakiness and Elongation Indices

Objective:

To determine the flakiness and elongation of the aggregates by standard flakiness gauge and elongation gauges.

Apparatus:

a) Flakiness Gauge (Thickness Gauge): The Flakiness index of aggregates is the percentages by weight of particles whose least dimension is less than three-fifths (0.6) of their mean dimension. The test is not applicable to sizes smaller than 6.3mm. The apparatus consists of a standard thickness gauge of IS sieve sizes 63, 50, 40, 31.5, 25, 20, 16, 12.5, 10 and 6.3mm and a balance to weigh the samples.



Fig3.7-Aggregates passing through F. G Fig3.8-Flakiness Gauge

b) Elongation Gauge (Length Gauge): The elongation index of aggregate is the percentage by weight of particles whose greatest dimension (length) is greater than one and four-fifths times (1.8) their mean dimension. The elongation test is not applicable to sizes smaller than 6.3mm. The apparatus consists of a standard-length gauge of IS sieve sizes 50, 40, 31.5, 25, 20, 16, 12.5, 10 and 6.3mm.



Fig3.9-Passing aggregates by Elongation gauge Fig3.10-Elongation Gauge

Procedure:

Flakiness Index: The sample is sieved with the sieves mentioned in above. A minimum of 200 pieces of each fraction to be tested is taken and weighed. To separate flaky materials, each fraction is then gauged for thickness on a thickness gauge. The amount of flaky material passing the gauge is weighed to an accuracy of at least 0.1 percent of the test sample.

Calculation:

To calculate the flakiness index of the entire sample of aggregates first the weight of each fraction of aggregate passing and retained on the specified set of sieves is noted (X1, X2, X3... etc.). Each of the particle from this fraction of aggregate is tried to be passed through the slot of the specified thickness of the thickness gauge are found and weighed (x1, x2, x3...etc.). Then the flakiness index is the total weight of the flaky material passing the various thickness gauges expressed as a percentage of the total weight of the sample gauged.

Elongation Index:

The sample is sieved through the IS sieves specified as above. A minimum of 200 pieces of each fraction is taken and weighed. To separate elongated material, each fraction is then gauged individually for length in a length gauge. The pieces of aggregates from each fraction tested which could not pass through the specified gauge length with its long side are elongated particles and are collected separately to find the total weight of aggregates retained on the length gauge from each fraction. The total amount of elongated material retained by the length gauge is weighed to an accuracy of at least 0.1 percent of the weight of the sample.

Calculation:

To calculate the Elongation index of the entire sample of aggregates first the weight of each fraction of aggregate passing and retained on the specified set of sieves is noted (Y1, Y2, Y3... etc.). Each piece of these is tried to be passed through the specified length of the gauge length with its longest side and those elongated pieces which do not pass the gauge are separated and weighed (y1, y2, y3...). Then the Elongation index is the total weight of the material retained on the various length gauges, expressed as a percentage of the total weight of the sample gauged.

Combined Flakiness & Elongation Index: To determine this combined proportion, the flaky stone from a representative sample should first be separated out. Flakiness index is weight of flaky stone metal divided by weight of stone sample. Only the elongated particle is separated out from the remaining (non-flaky) stone metal. Elongation index is weight of elongated particles divided by total non-flaky particles. The value of flakiness index and elongation index so found are added up.

Limits:

Flakiness Index for Bituminous and Non-bituminous Mixes = Max. 15%
 Elongation Index for Bituminous and Non-bituminous mixes = Max. 15%
 Combined Flakiness, Elongation Index for Bituminous & Non-bituminous mixes = Max. 30%
 Flakiness Index for Concrete mixes = Max. 35%

Table 3.3-Flakiness and elongation indices test report

FLAKINESS AND ELONGATION INDEX					
As per IS:2386 (Part-1)					
Sieve Size (mm)		FLAKINESS INDEX		ELONGATION INDEX	
Passing	Retained	Wt. Of the Fraction Gauged (gm)	Wt. Of material passing through Flakiness Gauge (gm)	Wt. Of the Fraction Gauged (gm)	Wt. Of the material returned through Elongation Gauge (gm)
63.0	50.0				
50.0	40.0				
40.0	31.5				
31.5	25.0				
25.0	20.0				
20.0	16.0	1225	255	970	139
16.0	12.5	832	82	750	87
12.5	10.0	658	78	580	85
10.0	6.3	230	55	175	36
	Total	2945	470	2475	347

Note: Minimum 200 pcs. Should be taken on each fraction for test.

Flakiness Index (%) : (B/A) X 100 =	15.96
Elongation Index (%) : (D/C) X 100 =	14.02
Combined (EI+FI) (%) =	29.98

Specific gravity and Water absorption test Introduction:

The specific gravity of an aggregate is a measure of strength or quality of the material. The specific gravity test helps in the identification of stone.

Water absorption gives an idea of strength of aggregate. Aggregates having more water absorption are more porous in nature and are generally considered unsuitable unless they are found to be acceptable based on strength, impact, and hardness tests.

Object: To find the specific gravity & water absorption of aggregates by perforated basket.

Apparatus:

- A wire basket of not more than 6.3mm mesh or a perforated container of convenient size with thin wire hangers for suspending it from the balance.
- A thermostatically controlled oven to maintain temperature of 100 to 110°C.
- A container for filling water and suspending the basket.
- A balance of capacity about 5 kg, to weigh accurate to 0.5 g, and of such a type and shape as to permit weighing of the sample container when suspended in water.
- A shallow tray and two dry absorbent clothes, each not less than 750 X 450 mm.



Fig3.11-Specific Gravity Machine



Fig3.12-Different Size of Aggregates

Procedure:

About 2 kg of the aggregate sample is washed thoroughly to remove fines, drained, and then placed in the wire basket and immersed in distilled water at a temperature between 100 to 120°C with a cover of at least 50mm of water above the top of the basket. Immediately after immersion the entrapped air is removed from the sample by lifting the basket containing it 25mm above the base of the tank and allowing it to drop 25 times at the rate of about one drop per second. The basket and the aggregate should remain completely immersed in water for a period of 24 +/- 0.5 hours afterwards.

The basket and the sample are then weighed while suspended in water at a temperature of 220 to 320°C. In case it is necessary to transfer the basket and the sample to a different tank for weighing, they should be jolted 25 times as described above in the new tank to remove air before weighing. This weight is noted while suspended in water W_1 g. The basket and the aggregate are then removed from water and allowed to drain for a few minutes, after which the aggregates are transferred to one of the dry absorbent clothes. The empty basket is then returned to the tank of water, jolted 25 times and weight in water W_2 gm.

The aggregates placed on the absorbent clothes are surface dried till no further moisture could be removed by this cloth. Then the aggregates are transferred to the second dry cloth spread in a single layer, covered, and allowed to dry for at least 10 minutes until the aggregates are completely surface dry. 10 to 60 minutes drying may be needed. The aggregates should not be exposed to the atmosphere, direct sunlight or any other source of heat while surface drying. A gentle current of unheated air may be used during the first ten minutes to accelerate the drying of aggregate surface. The surface dried aggregate is then weighed W_3 g. The aggregate is placed in a shallow tray and kept in an oven maintained at a temperature of 110°C for 24 hours. It is then removed from the oven, cooled in an airtight container, and weighed W_4 g. At least two tests should be carried out, but not concurrently.



Fig3.13- Oven Machine

Table3.4-Test Report of Specific Gravity and Water Absorption

SPECIFIC GRAVITY AND WATER ABSORPTION TEST						
S.No.	Determination		Trial I	Trial II	Trial III	Average
1	Wt. Of Dry Sample [SSD] [gms]	A	509.0	514.0	511.0	
2	Wt. Of Pycnometer + Water [gms]	B	1631.0	1631.0	1631.0	
3	Wt. Of Pycnometer + Water + Sample [gms]	C	1969.0	1968.0	1970.0	
4	Wt. of Oven Dry Sample [gms]	D	500.0	505.0	503.0	
5	Water Absorption [%]	$[(A-D)/D]*100$	1.80	1.78	1.59	1.72
6	Specific Gravity	$D/(A-[C-B])$	2.924	2.853	2.924	2.901
7	Average 3. Specific Gravity	$D/(D-[C-B])$	3.086	3.006	3.067	3.053

Limits:

The specific gravity of aggregates ranges from 2.5 to 3.0 The water absorption of aggregates ranges from 1 to 4.0%

Table3.5- Test Result and Limits

Description of Test	Test Method	Test Results	MORTH Standards
Aggregate impact value	IS2386 Part 4 & MORTH	26.66_	Maximum 30%
Combined flakiness and elongation indices	IS2386 Part 1 & MORTH	29.98_	Maximum 35%
Water absorption	IS2386 Part 3 & MORTH	1.72_	2.5% to 3%
Specific gravity test	IS2386 Part 3 & MORTH	3.053_	0.1% to 4%

EMULSION

Bitumen emulsion is one of the binding materials that can be used in the construction, maintenance of road, pavement, and highways. As per IRC 37-2012 we will use emulsion as a binder in my mix proportion.

Bitumen emulsion is a dispersion of fine minute droplets of bitumen into water manufactured by using emulsifying agents to emulsify bitumen in water. A major objective of using bitumen emulsions is to obtain a product that can be used without heating.

Benefits and Issues with Bitumen Emulsion Advantages of using bitumen emulsions include:

- They can be used with damp aggregates.
- Elevated temperatures are not required for proper use and application.
- They provide economic, environmental, and sustainable benefits.



Fig3.14- Sampling of Bitumen Emulsion from Stock Yard

Tests can be conducted as per IS8887-2004

1. Residue content of emulsion by evaporation (% by mass)
2. Penetration value of residue content of emulsion

Table 3.6-Test Results and Limits

Description of Test	Test Method	Test Result Obtained	Requirements of IS: 73-2013
Residue content of emulsion by evaporation (% by mass)	As per IS	60.46	60 minimum
Penetration value of residue content of emulsion	8887-2004	89.00	60 to 120

3.3 Cement

Cement or lime would use as a filler in cold mix design, it is performed very important role if recycled material contaminated with clay.

Cement was used as a filler material in this mix design. Cement is the important binding material in today's construction world, Ordinary Portland Cement (OPC) 43 grade confirming to IS: 8112-2013 cement used. Cement samples were collected from cement store of batching plant at Dobhi camp and tests were performed in site laboratory.

Test performed on Cement:-

1. Consistency of cement [As per IS: 4031 Part-4]
2. Initial Setting Time [As per IS: 4031 (Part-5) -1988]
3. Final Setting Time [As per IS: 4031 (Part-5) -1988]
4. Fineness of cement [As per IS: 4031 (Part-1) -1996]

3.3.1 Consistency of Cement [As per IS: 4031 Part-4]

Object: Determination of the quantity of water required to produce cement paste of standard consistency.

Apparatus: Vicat apparatus (confirming to IS: 5513-1968) with plunger (10mm dia).



Fig3.15-Vicat Apparatus

Theory:

The standard consistency of cement paste is defined as that consistency which will permit the vicat plunger to penetrate to a point 5 to 7 mm from the bottom of the vicat mould, when the cement paste is tested as described in the following procedure.

Procedure:

- Prepare a paste of weighted quantity of cement (400 gms) with a weighted quantity of water, start with 30% water of 400 gms of cement taking care that the time of gauging is not less than 3 minutes and not more than 5 minutes and the gaugings shall be completed before any sign of setting occurs.
- The gauging time shall be counted from the time of adding the water to the dry cement until commencing to fill the mould. Fill the vicat mould with this paste, the mould resting upon a non-porous plate. After completely filling the mould, trim off the surface of the paste, making it in level with the top of the mould. The mould may be slightly shaken to expel the air.
- Place the test block with the mould, together with the non-porous resting plate, under the rod bearing the plunger (10 mm dia) lower the plunger gently to touch the surface of the test block and quickly release, allowing it to penetrate into the paste. This operation shall carry out immediately after filling the mould.



Fig3.16-Sample of Cement

- Prepare trial pastes with varying percentages of water and test as described above until the amount of water necessary for making the standard consistency as defined above is obtained. Express the amount of water as a percentage by weight of the dry cement.



Fig 3.17-Preparing a Paste of Cement with Water

Precautions:

Use clean appliances for gauging. The temperature of cement and water and that of the room, at the time when the above operations are being performed, shall be $27^{\circ}\text{C} \pm 2^{\circ}\text{C}$. The room temperature shall be maintained at $27^{\circ}\text{C} \pm 2^{\circ}\text{C}$.

This test helps to determine the water content for other tests like initial setting time and final setting time.

3.3.2 Initial Setting Time and Final Setting Time

Object: Determination of the Initial and Final setting times of cement.

Apparatus: The vicat apparatus (conforming to IS: 5513 – 1968)

Sample: 350 gms of cement is taken.

Procedure:

Preparation of Test Block

Prepare neat cement paste by gauging 350 gms of cement with 0.85 times the water required to give a paste of standard consistency. The paste shall be gauged in the manner and under the conditions prescribed in determination of consistency of standard cement paste. Start a stopwatch at the instant when water is added to the cement. Fill the mould with the cement paste gauged as above, the mould resting on a non-porous plate, fill the mould completely and smooth off the surface of the paste making it level with the top of the mould. The cement block thus prepared in the mould is the test block.

In consistency test of cement, we add 120 ml of water in this test we add 85% of 120 ml that is 102 ml water is added to cement to become a paste.

Use clean appliances for gauging. The temperature of water and that of the test room, and the time gauging, shall be 270 C +/- 20 C.

During the test, the block shall be kept at a temperature of 270 C +/- 20 C and at not less than 90% relative humidity.

Determination of Initial Setting Time:

Place the test block confined in the mould and resting on the non-porous plate, under the rod bearing initial setting needle, lower the needle gently in contact with the surface of the test block and quickly release, allowing it to penetrate the test block. In the beginning the needle will completely pierce the test block. Repeat this procedure until the needle, when brought in contact with the test block and released as described above, fails to pierce the block for 5 +/-

0.5 mm measured from the bottom of the mould. The period lapsing between the time water is added to the cement and the time at which the needle fails to pierce the test block by 5 +/- 0.5 mm shall be the initial setting time.

Determination of Final Setting Time:

Replace the needle of the vicat apparatus by the needle with an annular ring. The cement shall be considered as finally set when, upon applying the needle gently to the surface of the test block, the needle makes an impression thereon, while the outer ring fails to do so. The period elapsing between the time when water is added to the cement and the time at which the needle makes an impression on the surface of the test block while the attachment fails to do so, shall be the final setting time.

Limits:

- Initial Setting Time, minimum-030 minutes.
- Final Setting Time, maximum-600 minutes.

3.3.3 Fineness of Cement [As per IS: 4031 (Part-1)-1996]

Object: To determine the fineness of cement by dry sieving.

Apparatus:

- a) Standard balance with 100 gm. weighing capacity.
- b) IS:90-micron sieve conforming to IS: 460-1962 and a Brush.

Procedure:

- Break down any air-set lumps in the cement sample with fingers.
- Weigh accurately 100 gms of the cement and place it on a standard 90 micron IS. sieve.

- Continuously sieve the sample for 15 minutes.
- Weigh the residue left after 15 minutes of sieving. This completes the test.

Result:

The percentage weight of residue over the total sample is reported.

$$\% \text{Weight of Residue} = (\text{Wt. Of Sample Retained on the Sieve} / \text{Total Weight of the Sample})$$



Fig3.18-Cement Test

Limits: The percentage residues should not exceed 10%.

Precautions: Sieving shall be done holding the sieve in both hands and gentle wrist motion, this will involve no danger of spilling the cement, which shall be kept well spread out on the screen. Continuous rotation of the sieve shall be carried out throughout sieving.

Washers, shots and slugs shall not be used on the sieve. The underside of the sieve shall be lightly brushed with a 25- or 40-mm bristle brush after every five minutes of sieving.

Mechanical sieving devices may be used, but the cement shall not be rejected if it meets the fineness requirement when tested by the hand method.

Table3.7-Cement Test Result and limit

Description of Test	Test Result Obtained	Requirements of IS: 8112-1989
Initial Setting Time	120 min	Min 30 Minutes
Final Setting Time	245	Max. 600 Minutes
Fineness	3.25%	Not more than 10%

3.4 Recycle Material (RAP):

Recycle material accumulated from PATNA to DOBHI (NH-83) highway existing bituminous pavement. Existing bituminous layer milled by cold recycling process upto 150mm and milled material transported to the Dobhi camp 3. Here recycled material stored in stockpile. Sample taken from stockpile for mix design trial and various test were performed in the site laboratory like as gradation of recycle material, aggregate impact value test, bitumen extraction from recycle material. Milling material shared maximum percentile of mix design hence it is necessary to assure the quality of recycle material before use as a main ingredient of mix design. If milling material contaminated with clay, then we are used 2 % lime as per IRC 37- 2012 but there is no situation arise for doing so.

RAP is the pulverized excavated material that has been recovered usually by milling that is used as an aggregate material for the rehabilitation and maintenance of roads. The use of RAP as an alternative to new virgin aggregate materials is gaining worldwide attention as a sustainable, economic, widely available, and environmentally friendly option. The RAP to be used should be properly tested and characterized to ascertain its properties that include the gradation, moisture content, density, elongation and flakiness index, the residual binder content, compatibility, penetration, and softening point of the residual binder in the RAP.



Fig3.19-StockyardsofRAP materials

Test performance on RAP materials

1. Aggregates Impact Value Test (AIV)
2. Bitumen Extraction Test

Table 3.8-AIV Test Report

AGGREGATE IMPACT VALUE					
AsperIS 2386-Part IV					
S. No	Determination	Trial I	Trial II	Trial III	Average
1	Total Wt. Of Oven-dried Sample (passing 12.5mm-Retained 10mm Sieve)-W1 [gms]	360.5	362.5	367.5	12.15%
2	Wt. Of Material Retained on 2.36mm after testing - W2 [gms]	315	320	323	
3	Wt. Of Material Passing on 2.36mm after testing - W3 [gms]	46	43	45	
4	Difference in weight after testing (W1-W2-W3)	0.0	0.0	0.0	
5	Aggregate Impact Value (%) = $(W3/W1) \times 100$	12.62	11.72	12.11	

Table 3.9-Bitumen Extraction Test Report

Bitumen Extraction Test				
Asper IRC SP-21				
Sr. No.	DESCRIPTION	OBSERVATION		
		1	2	3
1	Wt. of Sample Before Extraction (gms)	1560	1264	1204
2	Wt. of Filter Paper Before Extraction (gms)	8.66	9.83	6.91
3	Wt. of Filter Paper After Extraction (gms)	9.29	10.3	7.16
4	Wt. of Aggregate in Filter Paper (gms) = (3-2)	0.63	0.47	0.25
5	Wt. of Sample After Extraction (gms)	1509	1236	1151
6	Wt. of Bitumen in gms = 1-(4+5)	50.37	27.53	52.75
7	% of Bitumen = $(6/1) \times 100$	3.23	2.18	4.38
8	Average % of Bitumen	3.26		



Fig 3.20-Bitumen Extraction Test

3.5 Experimental Procedure

According to research, up to now, there is no hard and fast rule for formal mix design of Emulsion Treated RAP, and in that respect no hard procedure and quality control test on laying of Emulsion Treated RAP. Thus, in this research, some laboratory tests were performed to obtain some mechanical properties of this mix. Test performed on mix as per IRC-37 2012 and test performed on individual ingredients by their relevant IS code and specifications.

3.5.1. Mix Design Procedure

1. Mix Gradation: All accumulated samples from the stock pile & site have been dried first 24- hours then individual sample taken and gradation test were performed as per sieve designated in IRC 37 2012 Table IX-1.

Results were obtained from individual gradation are showing given below:

- 40 mm
- 20 mm
- Crusher dust
- RAP (Milling Material)
- Filler (cement)

Various trial has been made for getting optimize gradation like as blending were made in trial- 1 is 40 mm+RAP+crusher dust +Cement but this trial does not give a satisfactory result due to larger size aggregates fluctuated the result in huge frequency. Hence second trial were made with RAP + 20 mm + Stone dust + Filler.

Both natural and RAP samples were brought to required size and suitable grading required for subbase, base, and surface course as per MORTH specifications.

3.5.2 Samples of Different Compositions and Results

Samples of different compositions were prepared by adding different percentage of RAP materials (0% RAP, 10% RAP, 25% RAP, 35% RAP, 45% RAP and 60% RAP).

Table-3.10-Composition of Different Materials

Sample No.	Details of Composition
R1	RAP 0% + 95% Natural Aggregate + 5% Stone dust
R2	RAP 10% + 75% Natural Aggregate + 15% Stone dust
R3	RAP 25% + 58% Natural Aggregate + 17% Stone dust

R4	RAP35%+40%Natural Aggregate +25%Stonedust
R4	RAP45% +25%NaturalAggregate+30%Stonedust
R6	RAP60%+5%NaturalAggregate+35%Stone dust

Table3.11-TestResults Table

Sample Composition	Aggregate Impact Value	Flakiness & Elongation Index (Combined)	Loss Angeles Abrasion Test Value	Water Absorption
RAP 0% + 95% Natural Aggregate+5%Stonedust	26.5%	25.8%	31%	1.9%
RAP 10% + 75% Natural Aggregate+15%Stonedust	25%	23.2%	28.9%	1.82%
RAP 25% + 58% Natural Aggregate+17%Stonedust	22.2%	28.4%	26.2%	1.92%
RAP 35% + 40% Natural Aggregate+25%Stonedust	20.5%	24.6	25.4%	1.72%
RAP 45% + 25% Natural Aggregate+30%Stonedust	17.8%	20.5%	19.8%	1.10%
RAP 60% + 5% Natural Aggregate+35%Stonedust	18.9%	22.5	18.5%	1.63%

Table3.12-STANDARDWMM MIXEDDesign

	Aggregates Impact Value	Flakiness And Elongation Test	Loss Angeles Abrasion Test Value	Water Absorption
StandardWMM Mixed Design	21.70%	24.04%	23.8%	0.74%

3.5.2.1 Outcoming:

- From the test result as shown in table, it was observed that sample having composition of **RAP 45%, 20mm fine aggregate, Stone dust 30%** give the best result and follow the MORTH limit.
- Samplehavingcompositionof **RAP45%,20mmfine aggregate,Stonedust30%** canbe used in WMM layers for flexible pavements.
- From the test result as shown in table, it was observed that sample compositions of **RAP 45%, 20mm fine aggregates, Stone dust 30%** give best result and also follow the MORTH limit.

• **3.6 Blending**

Blending of all ingredients by through average individual gradation as follows:

Table 3.13-Grading Analysis of 20mm Down Aggregates (Sample-1)

20 mm					
SAMPLE-1					
GRADING ANALYSIS					
(As per: 2386, Part-1 & MORTH)					
IS Sieve Size (mm)	Material Retained (gms)	Cumulative Material Retained (gms)	% Retained cumulative	% Passing	Remarks
45	0	0	0.00	100.00	
37.50	0	0	0.00	100.00	
26.50	0	0	0.00	100.00	
19.00	2197	2197	23.75	76.25	
13.20	4364	6561	70.93	29.07	
4.75	2564	9125	98.65	1.35	
2.36	125	9250	100.00	0.00	
0.600	0	9250	100.00	0.00	
0.300	0	9250	100.00	0.00	
0.075	0	9250	100.00	0.00	

Table 3.14-Grading Analysis of 20mm Down Aggregates (Sample-2)

20 mm					
SAMPLE-2					
GRADING ANALYSIS					
(As per: 2386, Part-1 & MORTH)					
IS Sieve Size in mm	Material Retained (gms)	Cumulative Material Retained (gms)	% Retained cumulative	% Passing	Remarks
45	0	0	0.00	100.00	
37.50	0	0	0.00	100.00	
26.50	0	0	0.00	100.00	
19.00	2872	2872	20.41	79.59	
13.20	6948	9820	69.79	30.21	
4.75	4093	13913	98.88	1.12	
2.36	157	14070	100.00	0.00	
0.600	0	14070	100.00	0.00	

Table 3.15-Grading Analysis of 20mm Down Aggregates (Sample-3)

20 mm					
SAMPLE-3					
GRADING ANALYSIS					
(As per: 2386, part-1 & MORTH)					
ISSieveSize in mm	Material Retained(gms)	Cumulative Material Retained (gms)	%Retained cumulative	%Passing	Remarks
45	0	0	0.00	100	
37.50	0	0	0.00	100.00	
26.50	0	0	0.00	100.00	
19.00	3517	3517	23.12	76.88	
13.20	6823	10340	67.98	32.02	
4.75	4631	14971	98.43	1.57	
2.36	239	15210	100.00	0.00	
0.600	0	15210	100.00	0.00	
0.300	0	15210	100.00	0.00	
0.075	0	15210	100.00	0.00	

Table 3.16-Grading Analysis of 20mm Down Aggregates (Average)

AVERAGE % OF 20MM FRESH T AGGREGATES				
ISSieveSize (mm)	Trial-1	Trial-2	Trial-3	%Passing
45	100.00	100.00	100.00	100.00
37.50	100.00	100.00	100.00	100.00
26.50	100.00	100.00	100.00	100.00
19.00	76.25	79.59	76.88	77.57
13.20	29.07	30.21	32.02	30.43
4.75	1.35	1.12	1.57	1.35
2.36	0.00	0.00	0.00	0.00
0.600	0.00	0.00	0.00	0.00
0.300	0.00	0.00	0.00	0.00
0.075	0.00	0.00	0.00	0.00

3.6.2:RAP Material

Table3.17-GradingAnalysisofRAPMaterials(Sample-1)

SAMPLE-1					
RAPMATERIALS					
GRADINGANALYSIS					
(Asper2386, part-1&MORTH)					
ISSieveSize(mm)	Material Retained(gms)	Cumulative Retained(gms)	%Retained cumulative	%Passing	Remarks
45	0	0	0	100.00	
37.50	318	318	3.00	97.03	
26.50	476	794	7.50	92.50	
19.00	445	1239	11.70	88.30	
13.20	898	2137	20.18	79.82	
4.75	4733	6870	64.87	35.13	
2.36	1695	8565	80.88	19.12	
0.600	1200	9765	92.21	7.79	
0.300	236	10001	94.44	5.56	
0.075	544	10545	99.58	0.42	

Table3.18-GradingAnalysisofRAPMaterials(Sample-2)

SAMPLE-2					
GRADINGANALYSIS					
(Asper2386, part-1&MORTH)					
ISSieveSize in mm	Material Retained (gms)	Cumulative Material Retained(gms)	%Retained cumulative	%Passing	Remarks
45	0	0	0	100.00	
37.50	401	401	4.20	95.80	
26.50	258	659	6.90	93.10	
19.00	563	1222	12.80	87.20	
13.20	377	1599	16.74	83.26	
4.75	4549	6148	64.38	35.62	
2.36	1753	7901	82.73	17.27	
0.600	984	8885	93.04	6.96	
0.300	120	9005	94.29	5.71	
0.075	499	9504	99.52	0.48	

Table 3.19-Grading Analysis of RAP Materials (Sample-3)

SAMPLE-3					
GRADING ANALYSIS					
(Asper 2386, part-1 & MORTH)					
ISSieve Size in mm	Material Retained (gms)	Cumulative Material Retained (gms)	%Retained cumulative	%Passing	Remarks
45	0	0	0	100.00	
37.50	424	424	4.20	95.80	
26.50	212	636	6.29	93.71	
19.00	435	1071	10.60	89.40	
13.20	591	1662	16.45	83.55	
4.75	4718	6380	63.14	36.86	
2.36	1891	8271	81.85	18.15	
0.600	1142	9413	93.15	6.85	
0.300	35	9448	93.50	6.50	
0.075	607	10055	99.51	0.49	

Table 3.20-Grading Analysis of RAP Materials (Average)

AVERAGE % OF RAP MATERIALS				
ISSieve Size in mm	Trial-1	Trial-2	Trial-3	%Passing
45	100.00	100.00	100.00	100.00
37.50	97.00	95.80	95.80	96.20
26.50	92.50	93.71	93.10	93.10
19.00	88.30	89.40	87.20	88.30
13.20	79.82	83.55	83.26	82.21
4.75	35.13	36.86	35.62	35.87
2.36	19.12	18.15	17.27	18.18
0.600	7.79	6.85	6.96	7.20
0.300	5.56	6.50	5.71	5.92
0.075	0.42	0.49	0.48	0.47

3.6.3Crusher Dust

Table3.21-Grading AnalysisofCrusherDust(Sample-1)

CRUSHERDUST					
SAMPLE-1					
GRADINGANALYSIS					
(Asper2386,part-1&MORTH)					
ISSieve Size in mm	Material Retained (gms)	Cumulative Material Retained(gms)	%Retained cumulative	%Passing	Remarks
45	0	0	0.00	100	
37.50	0	0	0.00	100.00	
26.50	0	0	0.00	100.00	
19.00	0	0	0.00	100.00	
13.20	0	0	0.00	100.00	
4.75	0	0	0.00	100.00	
2.36	959	959	17.43	82.57	
0.600	2872	3831	69.63	30.37	
0.300	577	4408	80.12	19.88	
0.075	523	4931	89.62	10.38	

Table3.22-Grading AnalysisofCrusherDust(Sample-2)

CRUSHERDUST					
SAMPLE-2					
GRADINGANALYSIS					
(Asper2386,part-1&MORTH)					
ISSieveSize in mm	Material Retained (gms)	Cumulative Material Retained(gms)	%Retained cumulative	%Passing	Remarks
45	0	0	0.00	100	
37.50	0	0	0.00	100.00	
26.50	0	0	0.00	100.00	
19.00	0	0	0.00	100.00	
13.20	0	0	0.00	100.00	
4.75	6	6	0.34	99.66	
2.36	323	329	18.48	81.52	
0.600	944	1273	71.52	28.48	
0.300	184	1457	81.85	18.15	
0.075	171	1628	91.46	8.54	

Table 3.23-Grading Analysis of Crusher Dust (Sample-3)

CRUSHER DUST					
SAMPLE-3					
GRADING ANALYSIS					
(As per 2386, part-1 & MORTH)					
IS Sieve Size in mm	Material Retained (gms)	Cumulative Material Retained (gms)	% Retained cumulative	% Passing	Remarks
45	0	0	0.00	100	
37.50	0	0	0.00	100.00	
26.50	0	0	0.00	100.00	
19.00	0	0	0.00	100.00	
13.20	0	0	0.00	100.00	
4.75	29	29	1.75	98.25	
2.36	282	311	18.80	81.20	
0.600	859	1170	70.74	29.26	
0.300	170	1340	81.02	18.98	
0.075	161	1501	90.75	9.25	

Table 3.24-Grading Analysis of Crusher Dust (Average)

AVERAGE % OF CRUSHER DUST				
IS Sieve Size in mm	Trial-1	Trial-2	Trial-3	% Passing
45	100.00	100.00	100.00	100.00
37.50	100.00	100.00	100.00	100.00
26.50	100.00	100.00	100.00	100.00
19.00	100.00	100.00	100.00	100.00
13.20	100.00	100.00	100.00	100.00
4.75	100.00	99.66	98.25	99.30
2.36	82.57	81.52	91.20	85.10
0.600	30.37	28.48	29.26	29.37
0.300	19.88	18.15	18.98	19.00
0.075	10.38	8.54	9.25	9.39

The final blending percentage was obtained for dry ingredients.

Table 3.25-Analysis of Final Blending

Final Blending												
IS SIEVE (mm)	% of Passing				Percentage for Blending					IRC:37-2012 Table No. IX-1		
					20mm	RAP	Dust	Cement	Total % of Passing	Lower limit	MID LIMIT	Upper Limit
	20 mm	RAP	Dust	Cement	24%	45%	30%	1%	100%			
45.00	100.00	100.00	100.00	100.00	24.00	45.00	30.00	1.00	100.00	100.00	100.00	100.00
37.50	100.00	96.20	100.00	100.00	24.00	43.29	30.00	1.00	98.29	87.00	93.50	100.00
26.50	100.00	93.10	100.00	100.00	24.00	41.90	30.00	1.00	96.90	77.00	88.50	100.00
19.00	77.37	88.30	100.00	100.00	18.62	39.74	30.00	1.00	89.35	66.00	82.50	99.00
13.20	30.43	82.21	100.00	100.00	7.30	36.99	30.00	1.00	75.30	67.00	77.00	87.00
4.75	1.35	35.87	99.0	100.00	0.32	16.14	29.79	1.00	47.26	33.00	41.50	50.00
2.36	0.00	18.18	85.10	100.00	0.00	8.18	25.53	1.00	34.71	25.00	36.00	47.00
0.600	0.00	7.20	29.37	100.00	0.00	3.24	8.81	1.00	13.05	12.00	19.50	27.00
0.300	0.00	5.92	19.00	98.67	0.00	2.66	5.70	0.99	9.35	8.00	14.50	21.00
0.075	0.00	0.47	9.39	89.00	0.00	0.21	2.82	0.89	3.92	2.00	5.50	9.00

From the test results as shown in table, it was observed that sample composition of RAP 45%, 24% 20mm fine aggregates, Stone dust 30% and 1% give best result and also follow the MORTH limit.

And also, the final blending percentage of blending materials come under the limit in between lower limit and upper limit as per IRC:37-2012 Table No. IX-1 And also follow all limits of test results of materials under MORTH and IRC.

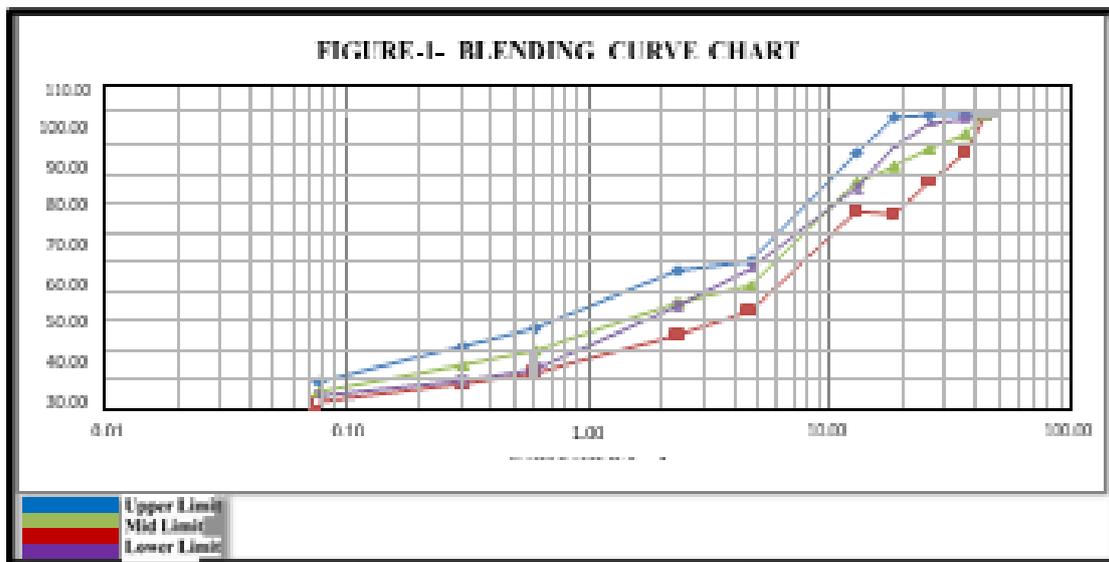


Fig.3.21-Blending Curve Chart

3.7.Determination ofMDD&OFC

These step gives an optimum fluid content on which mix can 100% compacted and density obtained onOFC is utilize at field compaction test as a maximum dry density of laboratory.

Fluidcontent of the mix is the sum of aggregate, moisture content, residual, bitumen content, water in the emulsion & additional water added to the mix.

The MDD & OFC were determined as per guidelines provided in IRC-37 2012 annexure-IX (in step 1,2,3) detailed description of the procedure is given below.

In this test we done 5 trial and each trail have 3 no. of 100mm diameter Mould cast. Take 1200gmbatchweightofdryingredients.Themixingwasdonefor1minutetoensureuniform & thorough coating of RAP & fresh virgin aggregate.

- Emulsion– 3%
- Water–2%
- 20mmaggregate -24%
- Stone dust – 30%
- Cement–1%(Use as afiller material)
- RAPmaterial–45%

Bythe helpofthesepcentage, wefound theweight ofthesematerials.



Fig3.22-100mm dia Mould

- ActualmoisturecontentoftheblendofRAP,fillerandvirginaggregatewas determinedasperASTM 2216 guidelines. This is designated as a blend moisture content.
- 50:50blendofemulsion&watermixbyvolumewasprepared. Waterisaddedtothe

bitumen emulsion because if we add the emulsion into the water, premature breaking takes place. So, prevent premature breaking, water added into the emulsion.

- Take 1200 grams' batch weight of dry ingredients. The mixing was done for 1 minute to ensure uniform & thorough coating of RAP & fresh virgin aggregate.



Fig3.23-Mixing of materials for casting of Mould

- Clean a Marshall Mould of 100mm dia. and oiling done on inner surface.
- Mix put into Mould and compacted with 75 blows on one face by manual compaction, reverse the Mould & base plate compaction process with 75 blows are performed on other face.
- Remove the Marshall Mould from the compactor. And similar 3 Mould were casted on each fluid content.
- Same Mould were casted at every fluid content increment of 1%. The increment in fluid content was by additional of extra water to the blend of Rap & virgin aggregate. Three Marshall specimens on each individual fluid content of 5%, 6%, 7%, 8% & 9% were casted.
- After 24 hours the specimens were ejected from the Mould by Marshall machine and evaluated for their bulk density as ASTM D 272 6.

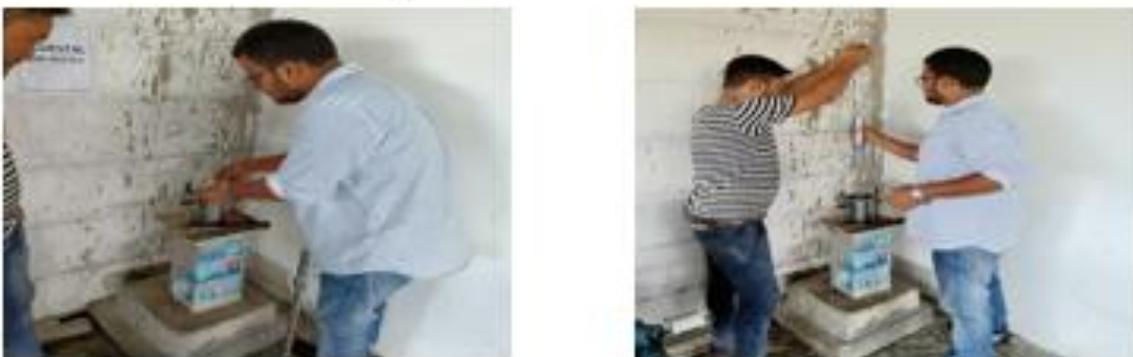


Fig3.24-Pedestal Hammer

- A graph was plotted between the calculated dry densities and corresponding total fluid contents. The MDD & OFC was determined from the graph. OFC obtained from the drawing the vertical line corresponding from Maximum density. The calculated mean dry density at different fluid contents is given in table and the graph were replotted between the dry density & corresponding fluid contents is shown in figure.

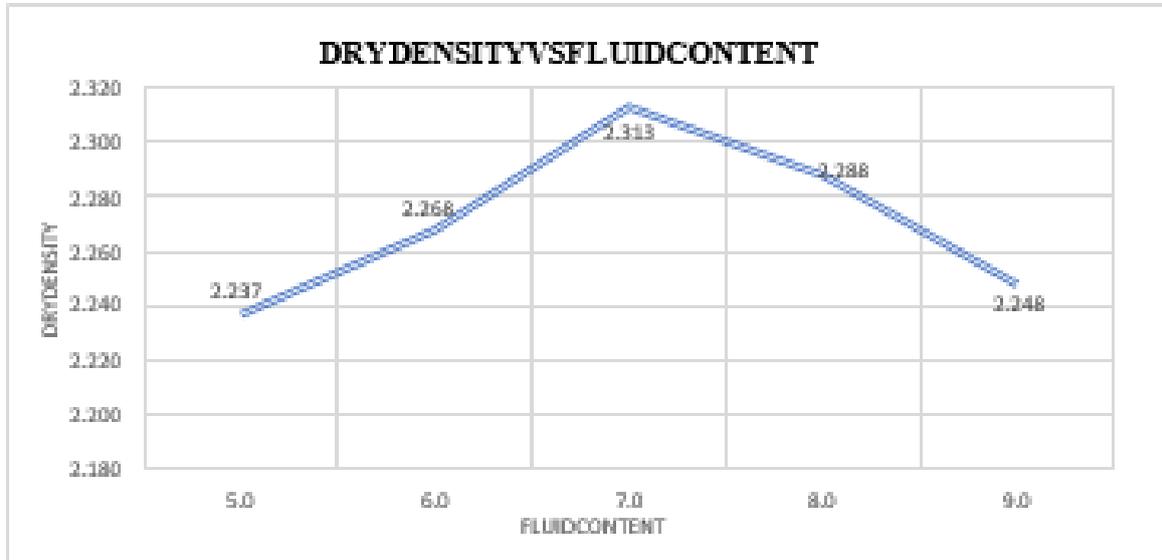


Fig3.25-Dry Density and Fluid Content

Table 3.25-Emulsion treated Reclaimed Asphalt Pavement Density Test

EMULSION TREATED RECLAIMED ASPHALT PAVEMENT														
Dry Density Test														
Specimen Identify No.	1	2	3	4	5	6	7	8	9	10	11	12	13	14
	% of Total Dry Weight of Sample	% of Total Dry Weight of Sample	% of Total Dry Weight of Sample	Total Weight of Sample (g)	Wt of Solids in Air (g)	Wt of Solids in Air (g)	Wt of Solids in Air (g)	Volume of solids in air (ml)	Wt of Solids in air (g)	Average Wt of Solids (g/ml)	Dry Weight of Sample (g)	Wt of Solids in Air (g)	% of Total Dry Weight of Sample	Dry Density (g/cm³)
A-1				5.00	1230.0	680.0	12240.0	534.0	2.285	2.277	1198.5	1.79	1.77	2.237
A-2	1.0	0.50	1.5		1212.0	685.0	12190.0	533.0	2.272		1191.0	1.76		
A-3					1218.0	687.0	12250.0	533.0	2.275		1197.0	1.75		
B-1				6.00	1231.0	706.0	12345.0	528.0	2.313	2.320	1198.0	1.92	1.92	2.276
B-2	1.0	0.50	1.5		1214.0	705.0	12250.0	517.0	2.346		1192.0	1.85		
B-3					1225.0	710.0	12425.0	512.0	2.300		1201.0	2.00		
C-1				7.00	1208.0	710.0	12150.0	502.0	2.405	2.389	1195.0	1.13	2.0	2.313
C-2	1.0	0.50	1.5		1218.0	700.0	12250.0	504.0	2.387		1192.0	2.06		

C-3					1279.0	689.0	0237.5	528.5	2.307		1085.0	2.87		
D-1	1.0	0.50	4.5	8.00	1225.0	706.0	0235.0	529.0	2.316	2.339	1095.0	2.50	2.2	2.288
D-2					1279.0	701.0	0235.0	534.0	2.326		1093.0	2.18		
D-3					1204.0	704.0	0231.0	507.0	2.375		1080.5	1.98		
E-1	1.0	0.50	1.5	9.00	1209.0	702.0	0212.0	500.0	2.339	2.510	1090.0	1.09	2.7	2.348
E-2					1230.0	701.0	0232.0	531.0	2.298		1086.0	2.87		
E-3					1225.0	702.5	0240.5	538.0	2.271		1072.5	4.30		

Table 3.26-Observation Table

OBSERVATION TABLE		
S.No.	DESCRIPTION	OBSERVATION
1	Emulsion Content%	3.00
2	Water Content%	3.5
3	Moisture Content in Blend Material %	0.5
4	Total Fluid Content%	7.00
5	Bulk density	2.359
6	Dry Density (gm/cc)	2.313

Outcome: Maximum Dry Density is 2.313 gm/cc found at 7.0% Fluid Content.

3.8 Indirect Tensile Strength (ITS)

Indirect tensile strength criteria on which trial mixes depend. If any mix satisfied the minimum required indirect tensile strength which is mentioned in IRC-37-2012 table no. IX-2 in both condition (dry & wet) then mix called design mix.

For indirect tensile strength some Mould preparation Test procedure areas follows-

Step-1 First of all, collect all required Marshall mould and other related equipment then thoroughly cleaned and inner surface greasing were done on mould.

Step-2 Take a 1200 gm batch of blended dry sample and according to the batch weight first take the emulsion & water mix which is equal to the OFC obtained in previously performed MDD & OFC test.

Emulsion may vary from 3 to 4 % by weight of total mix in increment of 0.5 %. Additional water is added to the first and mixed then the bitumen emulsion is added and mixed again approx. 1 minutetaken in mixing process, so mix become uniform and coating done on each

Step-3 After mixing, mix poured into the Marshall Mould on which filter paper already placed on base plate. By using trowel or straighted get top of specimen leveled, and another filter paper placed on top. So mix particle not stuck off by the hammer bottom.



Fig3.26-Mix poured into the Marshall Mould

Step-4 Prepared mix Mould placed in the compactor and gives 75 blows on one face & reverse the Mould & placed again, then again compacted by 75 blows on other face. Prepared six specimens of each emulsion percentage.

Step-5 Take the casted specimen with Mould and were cured in the Mould at room temperature for 24 hours.

Step-6 After 24 hours the specimens were extruded from the Mould. Here we are using marshal machine to remove the specimen from the Mould.

Step-7 All specimen evaluated for their bulk density as per ASTM D 2726. Then the specimen was cured in hot air oven maintained at 40°C for 72 hours.

Step-8 After completion of curing period, three cured specimens were tested for their dry ITS as per ASTM D 6931 @ 25°C temperature.

Following procedure adopted for ITS testing:

- Place cured specimen in the center of modified breaking apparatus.
- Check the apparatus placed in the center.
- Proving ring & dial gauges set on apparatus, at zero reading or initial reading was noted down.
- Start the marshal machine, which is operated at the speed of 55 mm/min.
- Take the highest reading of proving ring & corresponding dial gauge reading were taken.

Step-9 Another 3 cured specimen placed in water for 24 hours to perform ITS test in wet condition. Take the specimen after 24 hours, and performed the test similarly mentioned in step-8 and note down both ITS value in dry & wet condition.

Step-10 Similarly follow all step on different emulsion content and average ITS value of each emulsion percent note down. All ITS test parameter shown in given table.

- Noted highest proving reading in division it is converted into load by calibrating chart.
- Take the load reading in Newton and placed in the following formula which is mentioned in IRC-37- 2012-Equation IX-2 i.e.

$$ITS(KPa) = \frac{200 \times P_{max}}{\pi DH}$$

ITS=Indirect Tensile Strength in Kpa

P_{max} = Maximum Load in Newton

H= Thickness of the specimen

D=Dia of specimen

The design emulsion content is the optimum mix emulsion content which is satisfying the minimum ITS strength required given in table IX-II of IRC-37-2012, Annexure-IX.

By observing the ITS results presented in table no.28.

Table 3.27-Indirect Tensile Strength

State Moist of Test Results													
Proving Ring capacity (kN)											50		
Proving Ring per division value (kg)											7.03		
	% of Total Bit.	% of Binder in Control Mix	% of Water in Control Mix	Total % of Fluid in Control	Average Weight Specimen (mm)	No. of Specimen tested	ITS in condition	Proving Ring Reading	Stability (kg)	Stability Percent	Instability (kg)	Average Stability (KPa)	Minimum Strength as per IRC-37-2012 Table no. IX-2
A-1					64.0			40	344	1079	100		
A-2	1.00	0.5	3.50	7.0	65.0	100.0	ITS _{dry}	40	304	1003	104	304.03	
A-3					66.0			41	288	1028	173		
B-1					68.0			56	394	1062	162		
B-2	1.50	0.5	3.00	7.0	66.0	100.0		37	401	1001	179	366.94	>221 KPa
B-3					66.0			54	380	1034	160		
C-1					67.0			46	337	1000	115		
C-2	1.00	0.5	3.50	7.0	65.0	100.0	50	352	1040	108	321.60		
C-3					66.0		47	330	1001	113			
D-1					65.0		22	133	1017	140			
D-2	1.00	0.5	3.50	7.0	64.0	100.0	26	183	1793	170	161.60		
D-3					67.0		34	160	1403	137			
E-1					67.0		31	208	2128	203			
E-2	1.50	0.5	3.00	7.0	67.0	100.0	29	264	2000	190	193.40	>100 KPa	
E-3					68.0		26	197	1831	161			
F-1					65.0		31	162	1900	150			
F-2	1.00	0.5	3.50	7.0	68.0	100.0	23	176	1724	161	153.72		

From observed data it is found that emulsion content of 3.5% gives the better result of ITS strength and also satisfies the mix criteria of table IX-II.

Table 3.28-Final conformity as per MORTH

Final Conformity														
Specimen Identity No.	Data Sheet of Test Results													
	Proving Ring capacity (KN)							50						
	Proving Ring graduation value (kg)							7.00						
	1	2	3	4	5	6	7	8	9	11		12	14	
% of Emulsion Content by Wt of Total Mix	% of Moisture Content by Wt of Total Mix (Blend Material)	% of Water Content to be deducted to Blend Material	Total % of fluid Content	Average Height of Specimen (mm)	Dia. Of Specimen (mm)	Stability	Flow Comp. Modulus (KPa)	Stability (Kg)	Stability (mm)	Stability (mm)	Average Stability (KPa)	Minimum Strength as per IRC 57-2012 Table no. IX-2		
I-1	3.50	0.5	3.00	7.0	68.0	303.0	ITS dry	56	394	3862	362	366.84	>1110 KPa	
I-2					66.0			57	401	3931	379			
I-3					66.0			54	380	3724	359			
I-1	3.50	0.5	3.00	7.0	67.0	303.0	ITS wet	33	258	2138	204	191.41	>1110 KPa	
I-2					67.0			29	304	2880	190			
I-3					68.0			28	297	2931	181			

As per Code provision if ITS dry is greater than 400 KPa & similarly ITS wet is less than 50% of the ITS dry.

3.9 Marshall Stability Test

Marshall stability test performed on specimen prepared (casted) with following design parameter:

- Emulsion SS2-3.5%
- Water-3.5%
- 20 mm- 24%
- Filler-1%
- Stoved w/ 30%
- Recycled material-45%

Six specimens casted on above blended percentage for Marshall stability test. Test performed at 22.2°C with Marshall machine operated at the speed of 5.5 mm/minute. The test done after 24 hours, three sampled directly tested for dry stability & remaining three samples soaked in water and obtained result are tabulated as below:

Table 3.29-Emulsion Treated Reclaimed Asphalt Pavement

Check For Marshall Test								
EMULSION TREATED RECLAIMED ASPHALT PAVEMENT								
Data Sheet of Test Results								
Proving Ring capacity (KN)	50							
Proving Ring per division value (Kg)	7.03							
Specimen Identity No.	1	2	3	4	5	6	7	8
	% of Emulsion Content By Wt of Mix	% of Water Content By Wt of Mix x	Proving Ring Reading (KN)	Corrected stability for Proving Ring (Kg)	Average Stability (Kg)	Average Stability (KN)	Marshall Flow (mm)	Average Marshall Flow (mm)
In dry condition								
A-1	3.0	4.0	55	387	384	3.770	3.00	3.25
A-2			57	401			3.25	
A-3			52	366			3.15	
B-1	3.5	3.5	66	464	450	4.414	3.35	3.56
B-2			64	450			3.75	
B-3			62	436			3.60	
C-1	4.0	3.0	54	380	394	3.862	3.85	3.75
C-2			56	394			3.90	
C-3			58	408			3.40	
In soaked condition								
A-1	3.0	4.0	30	211	211	2.069	3.00	1.75
A-2			28	197			3.25	
A-3			32	225			3.15	
B-1	3.5	3.5	33	232	248	2.437	3.35	2.50
B-2			38	267			3.75	
B-3			35	246			3.60	
C-1	4.0	3.0	28	197	185	1.816	3.85	2.00
C-2			25	176			3.90	
C-3			26	183			3.40	

Table 3.30-Conformity Check

CONFIRMITY CHECK		
PARAMETER	RESULT	As per MORT & H Table No. 500-45 and MS -14 appendix-F
Maximum stability obtained @ 3.5% Emulsion & 3.5% Water content	4.414 KN	Min 2.2 KN at 22.2°C
Flow (mm)	4.25 mm	Min 2 mm

It is observed from the above table maximum stability found on 3.5 % emulsion content that is optimum value of emulsion content which is satisfied all criteria's mentioned in MORT & H Table No. 500-45 and MS-14 appendix Flow also satisfied minimum criteria mentioned in MORTH Table-45.

On comparing the results of emulsion treated Reclaimed Asphalt Pavement and DBM mixed design and it is observed that emulsion treated reclaimed asphalt pavement is not used on national highway where traffic load is very high. But it is used on service road as a DBM layer and where also traffic load is low.

Table 3.31-Test Result And Comparison

Test Results Comparison with MORTH Guidelines & Standard DBM (Grade-I)				
PARAMETER		RESULT	Standard DBM Grade-I	As per MORTH Standard
Tensile Strength (KPa)	Dry	333.24		> 325 KPa
	Soaked	424.74		> 300 KPa
Stability Number (KN)		4.414 KN	4.22 KN	Min 1.2 KN @ 22.2°C
FLOW value (mm)		4.25 mm	4.2 mm	Min 2 mm

Outcomings

- From the test result as shown in table, it was observed that Emulsion treated RAP (RAP 45%, 20mm fine aggregate, Stone dust 30%, 3% Emulsion & 4% Water) give the best result and follow the MORTH guidelines & result of Standard DBM Grade-I.
- Proposed Emulsion treated RAP mix design can be used in DBM Layers for Service roads and low traffic load roads.

CHAPTER:-4

4. RESULT AND DISCUSSION

4.1 Use of Reclaimed Asphalt Pavement design mix in WMM Layer

The samples having different compositions were prepared by adding different percentage of RAP materials (0% RAP, 10% RAP, 25% RAP, 35% RAP, 45% RAP and 60% RAP).

Table 4.1-Composition of Different Materials

Sample No.	Details of Composition
R1	RAP 0%+95% Natural Aggregate +5% Stone dust
R2	RAP 10%+75% Natural Aggregate +15% Stone dust
R3	RAP 25%+58% Natural Aggregate +17% Stone dust
R4	RAP 35%+40% Natural Aggregate +25% Stone dust
R4	RAP 45% +25% Natural Aggregate+30% Stone dust
R6	RAP 60%+5% Natural Aggregate+35% Stone dust

Then, various standard tests are performed on samples and compared with MORTH specified WMM design mix

Table 4.2-Test Results Table

Sample Composition	Aggregate Impact Value	Flakiness & Elongation Index (Combined)	Loss Angeles Abrasion Test Value	Water Absorption
RAP 0% + 95% Natural Aggregate+5% Stone dust	26.5%	25.8%	31%	1.9%
RAP 10% + 75% Natural Aggregate+15% Stone dust	25%	23.2%	28.9%	1.82%
RAP 25% + 58% Natural Aggregate+17% Stone dust	22.2%	28.4%	26.2%	1.92%
RAP 35% + 40% Natural Aggregate+25% Stone dust	20.5%	24.6	25.4%	1.72%
RAP 45% + 25% Natural Aggregate+30% Stone dust	17.8%	20.5%	19.8%	1.10%
RAP 60% + 5% Natural Aggregate+35% Stone dust	18.9%	22.5	18.5%	1.63%

Table 4.3- STANDARD WMM MIXED Design

	Aggregates Impact Value	Flakiness And Elongation Test	Loss Angeles Abrasion Test Value	Water Absorption
Standard WMM Mixed Design	21.70%	24.04%	23.8%	0.74%

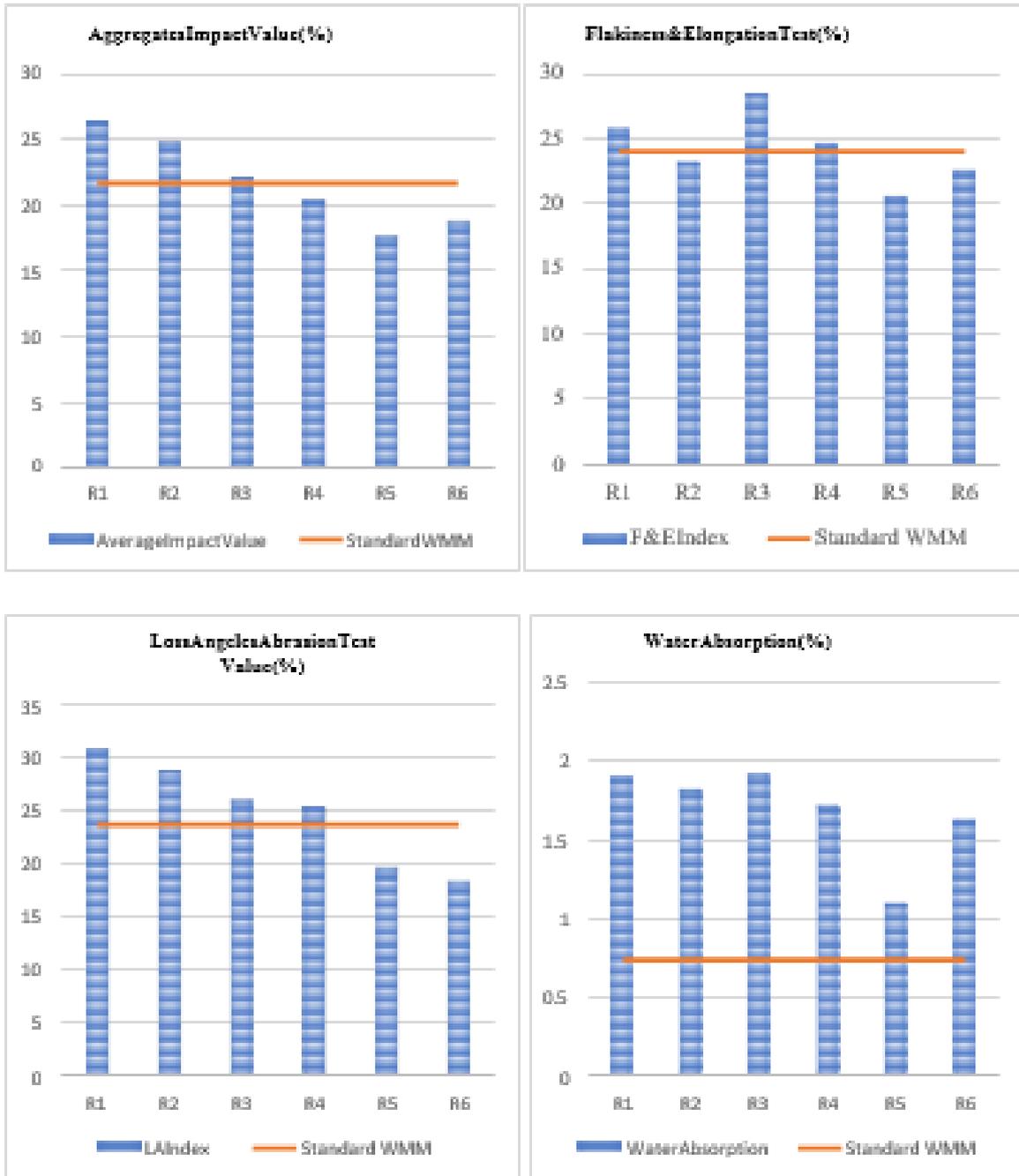


Fig 4.1- Result and comparison with standard WMM mixed Design.

Outcoming:

- From the test results as shown in table 4.3 and figure 4.1, it was observed that sample having composition of RAP 45%, 20mm fine aggregate 24%, Stone dust 30% and Cement 1% give the best result and follow the MORTH limit.
- Sample having composition of RAP 45%, 20mm fine aggregate 24%, Stone dust 30% and Cement 1% can be used in WMM layers for flexible pavements.

4.2 Use of Emulsion Treated Reclaimed Asphalt Pavement design mix in DBM

Layer 3.5% Emulsion and 3.5% water (Gross 7% Fluid Content) added in RAP 45%, 20mm fine aggregate, Stone dust 30% to get “Emulsion Treated Reclaimed Asphalt Pavement design mix” and then, various standard tests are performed on samples and compared with MORTH specified DBM design mix (Grade-I).

Table 4.4- Test Results Comparison

Test Results Comparison with MoRTH Guidelines & Standard DBM (Grade-I)				
PARAMETER		RESULT	Standard DBM Grade-I	As per MORTH Standard
Indirect Tensile Strength (KPa)	Dry	366.84	N/A	>225 KPa
	Soaked	191.41	N/A	>100 KPa
Stability Number (KN)		4.414 KN	4.81 KN	Min 2.2 KN @ 22.2 °C
FLOW value (mm)		3.56 mm	5.1 MM	Min 2 mm

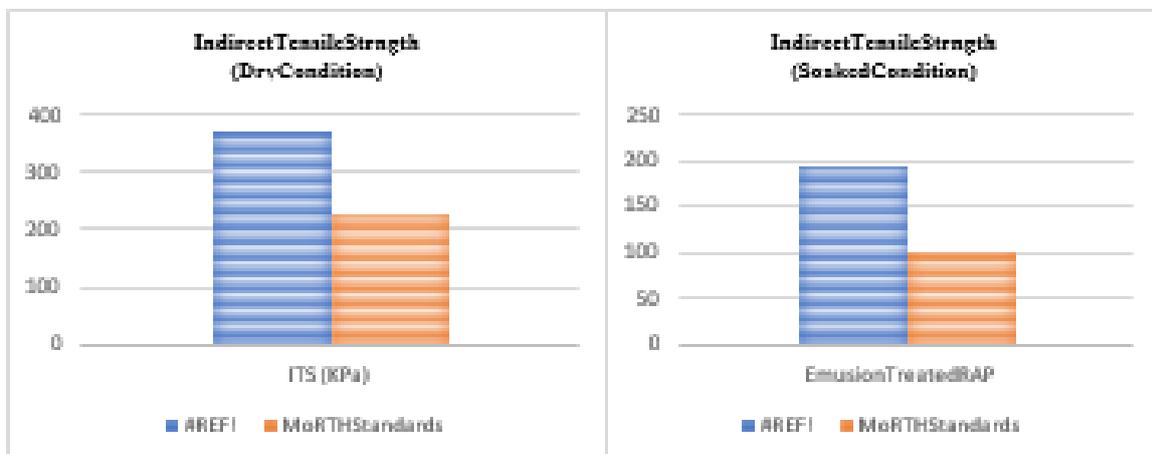


Fig 4.2- Result and comparison with standards MORTH specification

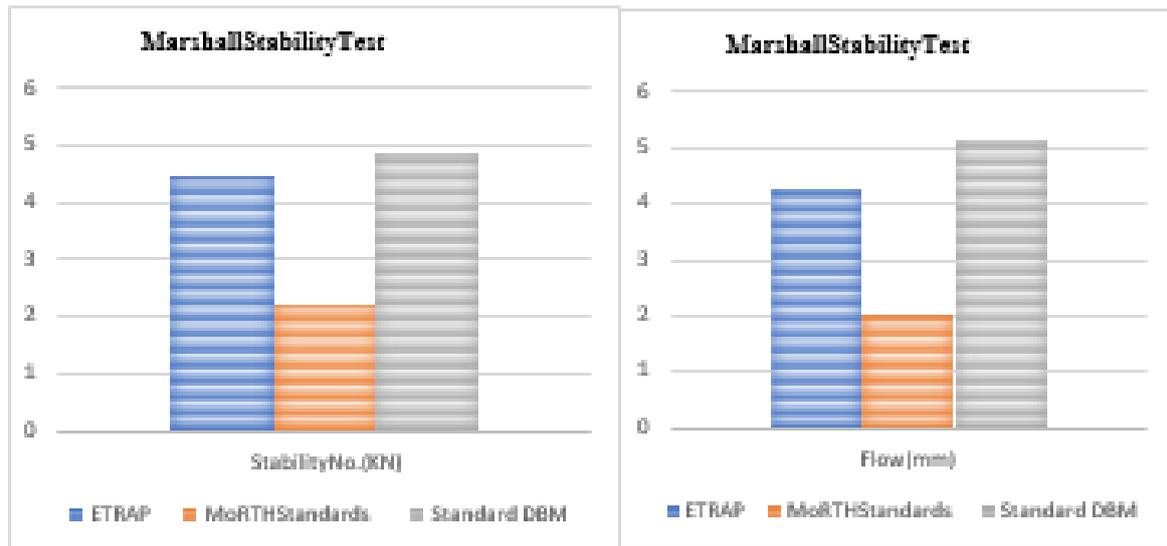


Fig4.3-ResultOfEmulsionTreatedRapAndComparisonWithMORTHStandards

From the test result as shown in table 4.4 and Fig-4.3, it was observed that Emulsion treated RAP(RAP45%,20mmfineaggregate,Stonedust30%,3%Emulsion&4%Water)give the best result and follow the MORTH guidelines & result of Standard DBM Grade-I. Therefore, Emulsion treated RAP mix design can be used in DBM Layers for Service roads and low traffic load roads.

CHAPTER:-5

5.1 RECOMMENDATIONS AND CONCLUSION

Based on study and experimental investigations following conclusions were drawn

- It was observed that the RAP materials can be successfully used in wet mix macadam layer and Dense bitumen macadam of flexible pavements after blending to match the required grading as per MORTH specifications for subbase material.
- It was also observed that the RAP materials in combination to natural aggregate in various proportions can be easily used after blending to match the required grading as per MORTH specifications in the base courses of flexible pavements.
- It is clear from the above investigation results that 20-30% replacement of natural aggregate can be successfully done in base course of flexible pavements, resulting in a savings of around 25- 30% in construction cost.
- It was observed that RAP has a higher content of fines as a result of degradation of material during milling and crushing operations it can be easily used for soil stabilization purposes to increase the CBR value of sub-grade and hence the crust thickness of road will be reduced resulting in reduction of cost of construction.
- Above all the problem of disposal of RAP wastes can be easily solved and adverse effect on environment may be avoided by using the RAP materials in flexible pavement construction.

10. REFERENCES

- [1] L. Allen Cooley, Jr., Ph.D. Kevin Williams, “P.E Development of Laboratory Mix Design Procedures for RAP Mixes”
- [2] Siksha Swaroopa Kar, Arvind Krishna Swamy, Devesh Tiwari, Dr. P. K. Jain “Review on Foam and Emulsion Based Cold Recycled Asphalt Mixes”.
- [3] IRCSP37-2012, “GuidelinesforTheDesignofFlexiblePavements(ThirdRevision)”
- [4] IRC120-2015, “RecommendedPracticeforRecyclingOfbituminousPavements”
- [5] MORTH(5threvisionsection500)[7]TG-2/MS-14(The designanduseofgranularemulsion mixes)
- [6] SP 20-2002: IRCRuralRoadManual.
- [7] Specification of Road & Bridge Work, Ministry of Shipping, Road Transport & Highway, Revision 4.
- [8] ISCodes: 2386, 2720.
- [9] IRC-37:2012, Tentative Guidelines for The Design of Flexible Pavement, Indian Road Congress, New Delhi.
- [10] Sunil S, K M Mallesh and T ChnadraSekharaiah, Experimental Investigations on the performance of Bituminous Mixes with Reclaimed Asphalt Pavement Material, International Journal of Research in Engineering and Technology, Volume 3, 2004.
- [11] Dr. B. B. Pandey, Cold Mix Recycling and Mix Design, Workshop on Recycling and other Pavements Rehabilitation Methods, 2005, 7-11, IIT Kanpur
- [12] S.K.KhannaandC.E.G.Justo,highwaymaterialtestingmanual.
- [13] Brajesh Mishra, “A Study on Use of Reclaimed Asphalt Pavement (RAP) Materials in Flexible Pavements, International Journal of Innovative Research in Science, Engineering and Technology, Vol. 4, Issue 12, December 2015.
- [14] SunilS,KMMalleshand T Chnadra Sekharaiah, Experimental Investigations on the

performance of Bituminous Mixes with Reclaimed Asphalt Pavement Material, International Journal of Research in Engineering and Technology, Volume 3, 2004.

[15] By V.K.L.Rao V.K.L.Rao M.Tech(GTE), MIE., MIRC., MIIBE., MICI., MIGS., CE
Senior Quality cum Material Expert-HIGHWAY MATERIAL TESTING MANUAL

[16] Masoud Faramarzi Case Study on Cement Treated Rap Containing Asphalt Emulsion and Acryl Polymer

[17] Md. Akhtar Hossain studied the Effect of Water Submergence on the Characteristics of Bituminous Mixes Using Reclaimed Asphalt Pavement.

[18] Burak Sengoz Stated the Performance Evaluation of Warm Mix Asphalt Mixtures with Recycled Asphalt Pavement.

[19] Maulik Rao Studied the utilization of recycled asphalt pavement in the Urban Area at Surat, Gujarat, India

[20] Baoshan Huang, Xiang Shu, Guoqiang Li (2005) are had done “Laboratory investigation of Portland cement concrete containing recycled asphalt pavements” this paper is they are used the RAP as aggregate in both fine and coarse, and conducted experimental study on its behavior.

[21] Athar Saeed (2008) had conducted study on the “Performance-Related Tests of Recycled Aggregates for Use in Unbound Pavement Layers”, this study is performing test on RAP

[22] Michael U. Bergin, Mang Tia, and Nabil Hossiney (2010)

[23] AASHTO, 1986. Guide for Design of Pavement Structures. American Association of State Highway and Transportation Officials, Washington.

[24] Asphalt Emulsion Manufacturers Association (AEMA), 2009. Basic Asphalt Emulsion Manual, Manual Series No. 19, Third Edition, USA

[25] Ahmad M. Abdo, Utilizing Reclaimed Asphalt Pavement (RAP) Materials in New Pavements. International Journal of Thermal & Environmental Engineering, Volume 12, No.1 (2016), pp. 61-66.